

UNIVERSITY OF LONDON

Chemical Engineering

E849

Answer **FIVE** questions only.

Each question carries a total of **25 marks** distributed as shown []

Additional stationery provided: graph paper

1. An air stream containing ammonia (NH_3) is to be purified by continuous counter-current contact with clean water in a packed tower. The inlet gas contains 7% by volume of ammonia of which 99% is to be removed. The ammonia-free mass flowrate of air is 5000 kg/h m^2 .

The equilibrium solubility of ammonia in water on a molar ratio basis is given by:

$$Y_A^* = 0.9 X_A$$

where Y_A^* is the mole ratio of ammonia in the gas phase and X_A is the mole ratio of ammonia in the liquid phase.

Calculate the following:

- a) the minimum liquid solvent flow rate [8]

- b) the required height of the packed column when the liquid solvent flow rate is 2 times the minimum and assuming that the mass transfer coefficient is $K_{OG}a = 300 \text{ kmol/h m}^3$ [17]

(average molecular weight of air = 29; molecular weight of ammonia = 17)

2. 10000 kg/hr of a mixture containing 40% (mole) methanol (CH_3OH) and 60% (mole) water (H_2O) is fed to a fractionating column to produce a distillate containing 90% (mole) methanol and a residue containing 90% (mole) water. The column is operating at 760 mmHg and is equipped with a total condenser and a partial reboiler. Assume that the feed, the distillate and the residue are all saturated liquids.

With the aid of a graphical construction on the diagram provided, which must be attached to your answer book, determine:

- a) enthalpies of feed, distillate and residue [2]
b) minimum reflux ratio R_{\min} [3]
c) number of theoretical stages for a reflux ratio $R = 1.5 R_{\min}$ [15]
d) condenser and reboiler thermal duties for a reflux ratio $R = 1.5 R_{\min}$ [5]

Data

Enthalpy-concentration diagram and a y-x diagram for the methanol-water system provided.

TURN OVER

3. A multicomponent light hydrocarbons mixture is to be fed as saturated liquid ($q=1$) into a tray tower operating at 2 atm in conjunction with a total condenser and a partial reboiler. The composition of the feed is given in Table 1. The distillate will have a content of n-pentane equal to a molar fraction of 0.05 and negligible n-hexane; the bottom product (residue) will have a content of n-butane equal to a molar fraction of 0.05 and negligible propane.

Table 1

All compositions are given in molar fractions	
	Feed (x_F)
1) propane	0.17
2) n-butane	0.32
3) n-pentane	0.35
4) n-hexane	0.16

Find the following:

- a) composition of distillate and residue [4]
 b) bubble point temperature of residue, and dew point temperature of distillate [15]
 c) minimum number of theoretical stages [6]

Data:

Relevant Antoine's constants are given in Table 2:

Table 2

	A	B	C
propane	15.72600	1872.46000	-25.16000
n-butane	15.67820	2154.90000	-34.42000
n-pentane	15.83330	2477.07000	-39.94000
n-hexane	15.83360	2697.55000	-48.78000

Antoine's Law: $\ln(P^\circ) = A - (B/(T+C))$

where: $[P^\circ = \text{mmHg}] [T = \text{K}]$

Fenske's Equation:

$$N_M + 1 = \frac{\ln \left[\left(\frac{x_{LK}}{x_{HK}} \right)_D \left(\frac{x_{HK}}{x_{LK}} \right)_B \right]}{\ln(\alpha_{LK})}$$

where:

- N_M = minimum number of theoretical stages in column
 q = heat to vaporize 1 mole of feed \div molar latent heat of feed
 α = relative volatility with respect to heavy key, computed as geometric mean of relative volatilities of distillate and residue streams
 x = liquid mol fraction
 F, D, B = feed, distillate and residue respectively
 LK, HK = light key and heavy key respectively

TURN OVER

4. An existing sieve tray is to be used to process a vapour flowrate of 4500 kg/h (density 2.85 kg/m³) and a liquid flowrate of 2800 kg/h (density 810 kg/m³). The column dimensions are as follows:

Tray type:	sieve tray - single pass	
Column diameter	D	0.80 m
Tray spacing	l _t	0.45 m
Weir height	h _w	38 mm
Weir length	l _w	0.56 m
Hole diameter	d _h	6 mm
Downcomer clearance	h _{ap}	38 mm
Column cross-sectional area	A _c	0.50 m ²
Downcomer area	A _d	0.05 m ²
Net area	A _n = A _c - A _d	0.45 m ²
Active area	A _a = A _c - 2A _d	0.40 m ²
Total hole area	A _h = 0.10A _a	0.04 m ²
Tray metal thickness	t	2.4 mm

Calculate the following:

- a) percentage flooding (% flooding)

[7]

Given:

$$\text{percentage flooding} = 100 \frac{u_n}{u_f}$$

where:

u_n is the actual gas velocity based on net area A_n

$$u_f = K_1 \sqrt{\frac{\rho_l - \rho_v}{\rho_v}}$$

(ρ_v and ρ_l are the densities of vapour and liquid respectively)

note that K₁ must be read from the chart provided after calculating the FLV factor:

$$F_{LV} = \frac{L_w}{V_w} \sqrt{\frac{\rho_v}{\rho_l}}$$

(L_w and V_w are the mass flow rates of vapour and liquid respectively, kg/s)

CONTINUED

b) total tray pressure drop (h_t) [mm] [7]

Given:

$$h_t = h_d + (h_w + h_{ow}) + h_r \quad [\text{mm}]$$

where:

$$h_d = \text{dry plate drop} = 51 (u_h/C_{vo})^2 (\rho_v/\rho_l) \quad [\text{mm}]$$

u_h is the actual gas velocity through holes, based on total hole area A_h

note that C_{vo} must be read from the chart provided

$$h_{ow} = \text{crest of liquid over the weir} = 750(L_w/(\rho_l l_w))^{0.667} \quad [\text{mm}] \quad (L_w \text{ as kg/s})$$

$$h_r = 12500/\rho_l \quad [\text{mm}]$$

c) height of liquid in the downcomer (h_b) [mm] [6]

Given:

$$h_b = (h_w + h_{ow}) + h_t + h_{dc} \quad [\text{mm}]$$

where:

$$h_{dc} = 166(L_w/(\rho_l A_{ap}))^2 \quad [\text{mm}] \quad (L_w \text{ as kg/s})$$

$$\text{and } A_{ap} = h_{ap} * l_w \quad [\text{m}^2]$$

d) downcomer residence time [5]

Given:

$$t_r = \frac{A_d h_b \rho_l}{L_w} \quad [\text{sec}] \quad (L_w \text{ as kg/s, } h_b \text{ as metre})$$

Data

Chart for calculating flooding velocity

Chart for calculating discharge coefficient C_{vo}

TURN OVER

5. a) Sketch how the *moisture content* of a drying solid varies with time [2]
- b) Write equations describing for the *drying rate* in terms of (i) the solid and (ii) the gas phases [2]
- c) Sketch how the batch drying rate varies with moisture content [2]
- d) Describe briefly, with reference to (a) and (c), the *constant drying rate* and *falling drying rate* periods [2]
- e) Show that the *total drying time* in a batch drier, θ_T , can be expressed by

$$\theta_T = \frac{L_S}{SN_{CR}} \left\{ (X_1 - X_C) + (X_C - X^*) \ln \frac{(X_C - X^*)}{(X_2 - X^*)} \right\}$$

where X_1 and X_2 are the moisture contents of the wet feed and dried product respectively, X_C and X^* are the critical and equilibrium moisture contents respectively, L_S is the mass of dry solid, S is the drying surface area, and N_{CR} is the constant drying rate.

State clearly any assumption that you may make.

- f) Twelve hours are required under constant drying conditions to reduce the moisture content of a wet solid from 24% to 6% with a critical moisture content of 12% and an equilibrium moisture content of 3%. How long would it take to dry a similar material from 36% to 9%? [12]

(All compositions are given on a dry basis)

TURN OVER

6. A power plant uses 360000 kg/h cooling water taken from a river nearby. After usage within the power plant, the cooling water has increased its temperature up to 40°C.

Environmental regulations impose that before the cooling water is discharged to the river it must be cooled down to 20°C. To this purpose, a forced draught countercurrent cooling tower is to be used.

Assuming that the wet bulb temperature of inlet air fed to the tower is 10°C and that the temperature of outlet air (nearly saturated) is 30°C, compute the following:

- a) Air flow rate flowing through the tower; [10]
- b) Number of gas transfer units (NTU), with the aid of a graphical construction on the graph paper supplied, which must be attached to your answer book. [15]

Data:

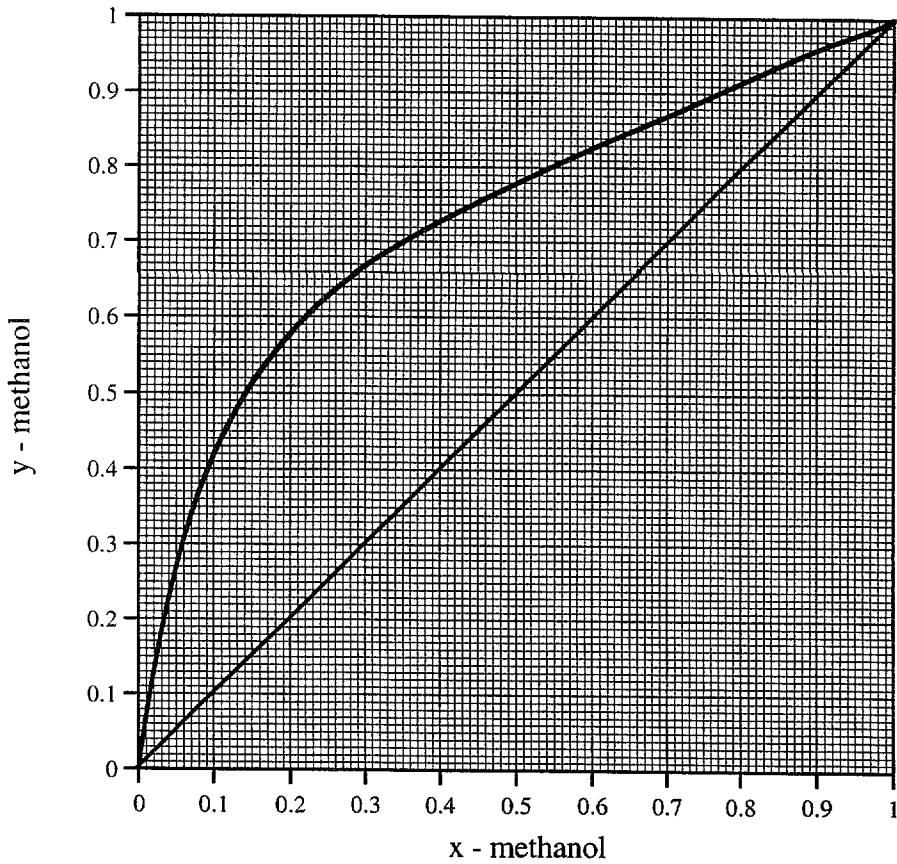
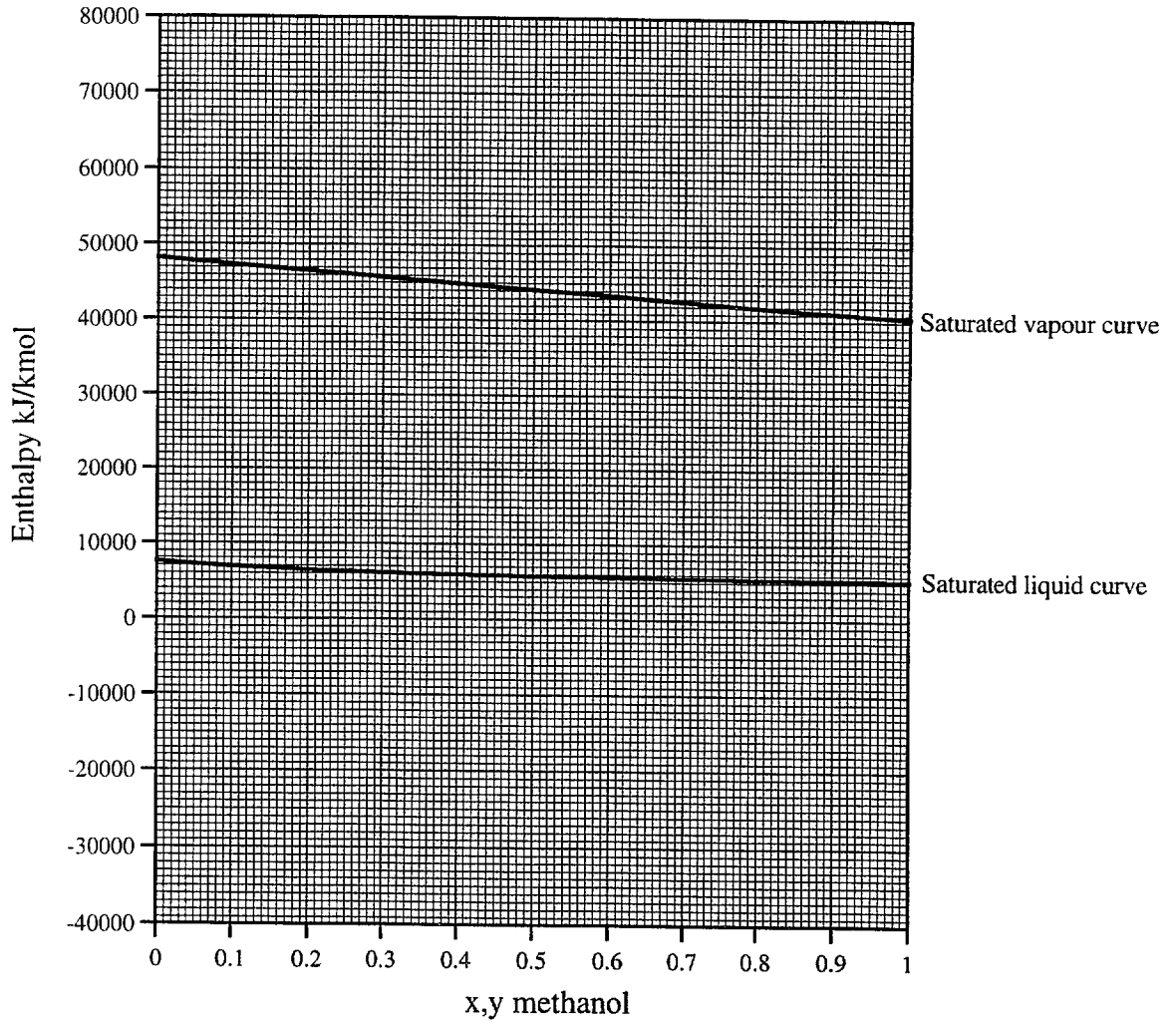
Heat capacity of liquid water: 4.19 kJ/kg °C

Saturated Air Temperature °C	10	15	20	25	30	35	40	45
Enthalpy of Saturated Air-Water vapour mixture (kJ/kg)	29.5	42.4	57.9	77	100.6	130.3	167.8	215.6

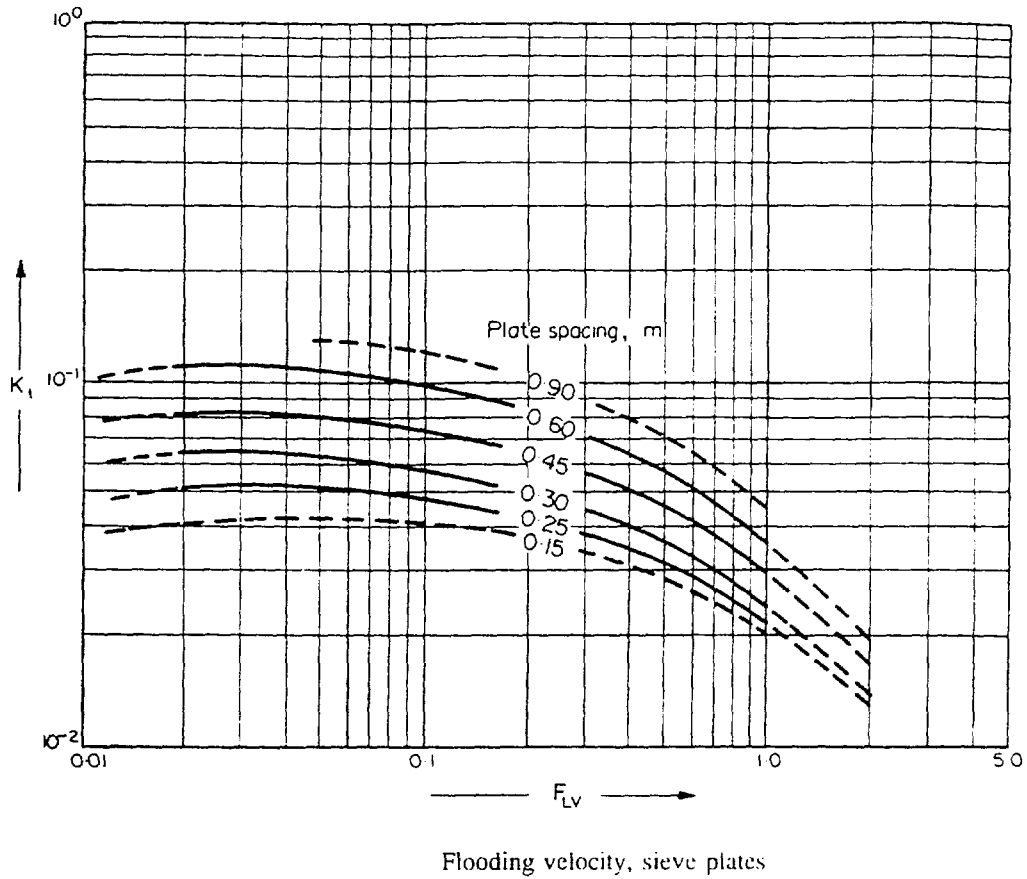
Standard graph paper to be supplied (A4 size)

TURN OVER

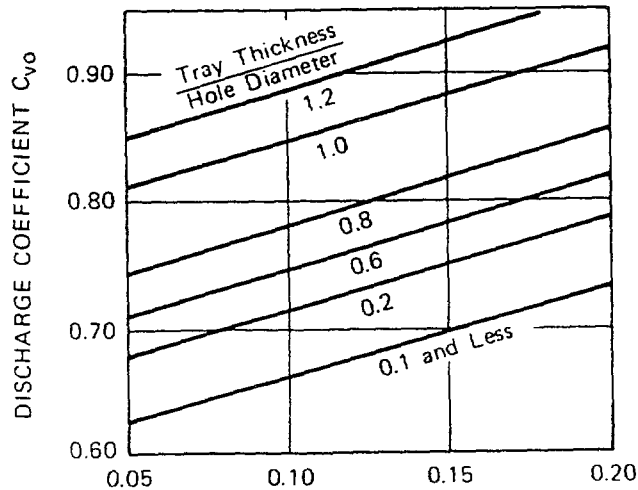
E-849 Exam paper 2002: Question number 2



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E 849 - 2002 EXAMS - QUESTION 4 - DIAGRAMS TO BE PROVIDED



$$\frac{\text{HOLE AREA}}{\text{ACTIVE AREA}} = \frac{A_h}{A_A}$$

Discharge coefficient for sieve trays.

END OF PAPER