

**MATH445001**

This question paper consists of 7 printed pages, each of which is identified by the reference **MATH445001**.

Only approved basic scientific calculators may be used.

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Examination for the Module MATH4450  
(May 2003)

**Polymeric Fluids**

Time allowed: **3 hours**

Answer FIVE of the SEVEN questions.

All questions carry equal marks.

1. Define the shear viscosity of a fluid in terms of the shear-stress and shear-rate. Explain the meaning of the terms shear-thinning and shear-thickening.

The stress  $\sigma$  in polymeric fluid is related to the shear-rate  $\dot{\gamma}$  by

$$\sigma + k^2 \sigma^3 = \eta \dot{\gamma},$$

where  $k$  and  $\eta$  are positive constants. Show that for small shear stresses,  $|\sigma| \ll 1/k$  that the fluid behaves as a Newtonian fluid with viscosity  $\eta$ . Show for  $|\sigma| \gg 1/k$  that fluid behaves as a power-law fluid and determine the index of the power-law. Sketch a graph of stress versus shear-rate for this material. Is it shear-thinning or shear-thickening?

This fluid is forced to flow down a channel of width  $2h$  by a pressure gradient of magnitude  $G$ . Show that the fluid velocity in the channel is given by

$$u = \frac{G}{2\eta} (h^2 - y^2) + \frac{k^2 G^3}{4\eta} (h^4 - y^4).$$

Find the volume flux per unit length,  $Q$

$$Q = \int_{-h}^h u dy,$$

and sketch a curve of  $\log Q$  versus  $\log G$  indicating the gradient at small and large values of  $G$ .

2. A polymeric fluid is contained between two parallel circular disks of radius  $a$  that are a distance  $h$  apart. The fluid is open to the atmosphere at  $r = a$ . The upper disk is rotated at angular velocity  $\Omega$  while the lower disk remains fixed, so that in cylindrical polar coordinates the fluid velocity between the plates is given by

$$\mathbf{u} = \frac{\Omega r z}{h} \hat{\boldsymbol{\theta}}.$$

Find the velocity gradient  $\mathbf{K}$  and show that for  $r \gg h$  the shear-rate  $\dot{\gamma}$  is approximately  $\frac{r\Omega}{h}$ . Define the normal stress differences  $N_1$  and  $N_2$  in this flow in terms of the components of the extra stress tensor  $\boldsymbol{\sigma}$ .

Hence show that a normal force equal to

$$F = 2\pi \int_0^a (\tau_{rr} + N_2 + p_{\text{atm}}) r dr$$

is required to maintain the separation of the plates, where  $p_{\text{atm}}$  is atmospheric pressure.

Show from the radial momentum equation that

$$\frac{\partial \tau_{rr}}{\partial r} = \frac{N_1 + N_2}{r}.$$

For the case  $N_1(\dot{\gamma}) = \Psi_1 \dot{\gamma}^2$  and  $N_2(\dot{\gamma}) = \Psi_2 \dot{\gamma}^2$  where  $\Psi_1$  and  $\Psi_2$  are constants, show that

$$\tau_{rr} = -p_{\text{atm}} + \frac{(\Psi_1 + \Psi_2)\Omega^2}{2h^2} (r^2 - a^2).$$

Hence find the force,  $F$ .

3. Write down an expression for the stress in a linear viscoelastic fluid of relaxation modulus  $G(t)$ . By considering the stress generated by a shear-rate,

$$\dot{\gamma} = \frac{d}{dt} (\epsilon \exp(i\omega t)),$$

define the complex modulus  $G^*$  and explain the significance of the real and imaginary parts of  $G^*$ .

The shear stress,  $\sigma(t)$  in a linear Maxwell fluid is related to the shear-rate  $\dot{\gamma}$  by

$$\tau \frac{d\sigma}{dt} + \sigma = \mu \dot{\gamma}.$$

Show that this is a linear viscoelastic fluid and find its relaxation modulus,  $G(t)$ .

Find the complex modulus of this fluid and show that the loss and storage moduli are given respectively by

$$G' = \frac{\mu\omega^2\tau}{1 + \omega^2\tau^2}, \quad G'' = \frac{\mu\omega}{1 + \omega^2\tau^2}.$$

A fluid satisfying the linear Maxwell model is subjected to the following shear flow

$$\dot{\gamma} = \begin{cases} a \sin \omega t & \text{for } t < 0, \\ 0 & \text{for } t \geq 0. \end{cases}$$

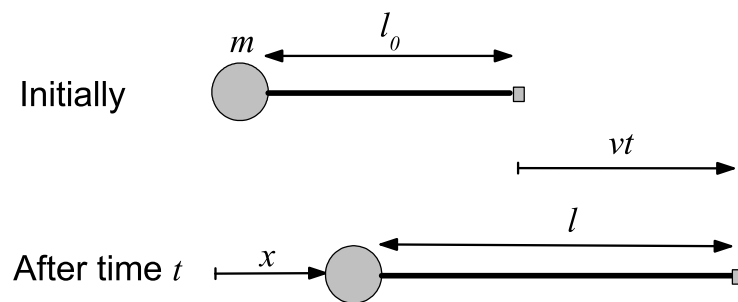
Find the shear stress for  $t > 0$ .

4. The expression for the total stress in a rubber is

$$\tau = G\mathbf{F} \cdot \mathbf{F}^T - \beta\mathbf{I}.$$

- (a) What is the deformation gradient  $\mathbf{F}$  and stress  $\tau$  for a volume-conserving uniaxial extension by a ratio  $\lambda$  in the  $x$ -direction? A piece of rubber, of initial cross sectional area  $A_0$ , is stretched by a ratio  $\lambda$ . If the sides of the rubber are exposed to the atmosphere, so that  $\tau_{yy} = \tau_{zz} = -p_{atm}$ , show that the force required to achieve the stretch is

$$f = GA_0 \left( \lambda - \frac{1}{\lambda^2} \right).$$



- (b) A mass  $m$  is attached to a thin piece of rubber of initial length  $l_0$  and initial cross sectional area  $A_0$ , as shown in the diagram. The other end of the rubber is initially held a distance  $l_0$  away (so that the rubber is just taught) and then moved away from the mass at constant velocity,  $v$ . Let  $x$  be the displacement of the mass from its initial position after time  $t$ .

- (i) By considering the length,  $l$ , of the rubber after time  $t$ , obtain expressions for the stretch,  $\lambda$ , of the rubber and the acceleration  $\frac{d^2x}{dt^2}$  of the mass (assuming that the only force on the mass is due to the rubber - i.e. it moves without friction)
- (ii) Defining  $X = x - vt$ , show that for small  $\frac{X}{l_0}$ ,

$$\frac{d^2X}{dt^2} = -\frac{3GA_0}{l_0m}X.$$

- (iii) Assuming the mass is initially at rest, obtain a solution for  $X$  (and hence,  $x$ ) as a function of time. For what velocities is the assumption of small  $\frac{X}{l_0}$  valid?
- (iv) Given that the rubber becomes “slack” for  $\lambda < 1$ , find the value of  $X$  at which this occurs. Show that this occurs first when

$$t = \pi \sqrt{\frac{3GA_0}{l_0m}}.$$

Briefly describe the subsequent motion of the mass.

5. Two particles, at positions  $x_1$  and  $x_2$ , are joined by a spring with spring constant  $k$  so that their Langevin equations are

$$\begin{aligned}\zeta \frac{dx_1}{dt} &= k(x_2 - x_1) + f_1(t) \\ \zeta \frac{dx_2}{dt} &= k(x_1 - x_2) + f_2(t)\end{aligned}$$

and  $\langle x_\alpha(t) f_\beta(t) \rangle = k_B T \delta_{\alpha\beta}$  (where  $\alpha, \beta = 1$  or  $2$ ).

- (a) Defining the particle separation  $r = x_2 - x_1$ , show that

$$\zeta \frac{dr}{dt} = -2kr + f_2 - f_1$$

and obtain a similar equation for the centre of mass  $R = \frac{x_1 + x_2}{2}$ .

- (b) Defining  $Q = \langle r^2 \rangle$ , show that

$$\frac{dQ}{dt} = -\frac{4k}{\zeta} Q + \frac{4k_B T}{\zeta}$$

and obtain a similar equation for  $P = \langle R^2 \rangle$ .

- (c) Solve the equations for  $P$  and  $Q$  subject to initial conditions  $x_1 = x_2 = 0$ .

Show that the energy in the spring,  $U = \frac{1}{2}kr^2$  approaches an average value of  $\frac{1}{2}k_B T$ .

What is the diffusion constant for the centre of mass?

6. The Rouse equation for a polymer chain comprising beads with friction constant  $\zeta$  connected with springs of spring constant  $k$  is

$$\zeta \left( \frac{\partial \mathbf{r}_s}{\partial t} - \mathbf{v}(\mathbf{r}_s) \right) = k \frac{\partial^2 \mathbf{r}_s}{\partial s^2} + \mathbf{f}_s, s = 0..N$$

This is used to model a chain in a rubber network, by setting

$$\begin{aligned}\mathbf{r}_s &= \mathbf{r}_A \text{ at } s = 0, \text{ and} \\ \mathbf{r}_s &= \mathbf{r}_B \text{ at } s = N\end{aligned}$$

where  $\mathbf{r}_A$  and  $\mathbf{r}_B$  represent the positions of the crosslink points at the ends of the chain.

We suppose  $\mathbf{v}_A = \mathbf{v}(\mathbf{r}_{s=0}) = \frac{d\mathbf{r}_A}{dt}$  and  $\mathbf{v}_B = \mathbf{v}(\mathbf{r}_{s=N}) = \frac{d\mathbf{r}_B}{dt}$ , and that  $\mathbf{v}(\mathbf{r}_s) = \mathbf{v}_A + \mathbf{K} \cdot (\mathbf{r}_s - \mathbf{r}_A)$  where  $\mathbf{K}$  is the velocity gradient tensor.

- (a) Let  $\mathbf{r}_s = \mathbf{r}_A + \frac{s}{N}(\mathbf{r}_B - \mathbf{r}_A) + \mathbf{x}_s$ . Show that

$$\frac{\partial \mathbf{r}_s}{\partial t} - \mathbf{v}(\mathbf{r}_s) = \frac{\partial \mathbf{x}_s}{\partial t} - \mathbf{K} \cdot \mathbf{x}_s$$

and that

$$\frac{\partial^2 \mathbf{r}_s}{\partial s^2} = \frac{\partial^2 \mathbf{x}_s}{\partial s^2}$$

Hence, obtain a partial differential equation for the new variable  $\mathbf{x}_s$ . What are the boundary conditions on  $\mathbf{x}_s$  at  $s = 0$  and  $s = N$ ?

- (b) Ignoring the terms due to velocity gradient  $\mathbf{K}$  and random force  $\mathbf{f}_s$ , show that the relaxation time of the  $p$ th normal mode  $\mathbf{x}_s = \mathbf{X}_p \sin\left(\frac{\pi p s}{N}\right)$  is

$$\tau_p = \frac{\tau_1}{p^2}$$

where  $\tau_1 = \frac{N^2 \zeta}{\pi^2 k}$ .

- (c) Given that this model leads to a time-dependent modulus of form

$$G(t) = G_0 + G_0 \sum_{p=1}^{\infty} \exp\left(-\frac{p^2 t}{\tau_1}\right)$$

obtain approximations of the form  $G(t) = ct^\alpha$  for  $t \gg \tau_1$  and (by approximating the sum as an integral) for  $t \ll \tau_1$ . Hence sketch a graph of  $\log G(t)$  versus  $\log t$ . Why doesn't  $G(t)$  decay to zero?

You may use the result  $\int_0^\infty dX \exp(-X^2) = \frac{\sqrt{\pi}}{2}$ .

7. The constitutive equation for the Upper Convected Maxwell model is

$$\boldsymbol{\tau} = G\mathbf{A} - \beta\mathbf{I},$$

where the structure tensor  $\mathbf{A}$  satisfies

$$\frac{d\mathbf{A}}{dt} = \mathbf{K} \cdot \mathbf{A} + \mathbf{A} \cdot \mathbf{K}^T - \frac{1}{\tau}(\mathbf{A} - \mathbf{I}).$$

A fluid that obeys the Upper Convected Maxwell model is subjected to a transient shear flow  $\mathbf{u} = (\dot{\gamma}y, 0, 0)$  where

$$\dot{\gamma} = \begin{cases} 0 & \text{for } t < 0, \\ g & \text{for } t \geq 0. \end{cases}$$

Write down the equation for evolution of the tensor,  $\mathbf{A}$ , for  $t \geq 0$  and show that only the components  $A_{xx}, A_{xy}$  change with time. Find  $A_{xy}$  and  $A_{xx}$  as functions of time and show for  $0 < t \ll \tau$  that

$$A_{xx} \sim 1 + g^2 t^2.$$

Hence sketch a graph showing the first normal stress difference as a function of time.

## Formulae Sheet

### Cartesian coordinates

pressure,  $p$ , velocity,  $\mathbf{u} = u\mathbf{e}_x + v\mathbf{e}_y + w\mathbf{e}_z$ , velocity gradient,  $\mathbf{K}$  with  $K_{ij} = \frac{\partial u_i}{\partial x_j}$

$$\nabla p = \frac{\partial p}{\partial x}\mathbf{e}_x + \frac{\partial p}{\partial y}\mathbf{e}_y + \frac{\partial p}{\partial z}\mathbf{e}_z, \quad \nabla \cdot \mathbf{u} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z},$$

$$\mathbf{K} = \begin{pmatrix} \frac{\partial u}{\partial x} & \frac{\partial u}{\partial y} & \frac{\partial u}{\partial z} \\ \frac{\partial v}{\partial x} & \frac{\partial v}{\partial y} & \frac{\partial v}{\partial z} \\ \frac{\partial w}{\partial x} & \frac{\partial w}{\partial y} & \frac{\partial w}{\partial z} \end{pmatrix} \quad \nabla \cdot \boldsymbol{\sigma} = \begin{pmatrix} \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yx}}{\partial y} + \frac{\partial \sigma_{zx}}{\partial z} \\ \frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{zy}}{\partial z} \\ \frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} \end{pmatrix}$$

### Cylindrical Polar Coordinates

velocity,  $\mathbf{u} = u\mathbf{e}_r + v\mathbf{e}_\theta + w\mathbf{e}_z$ .

$$\nabla p = \frac{\partial p}{\partial r}\mathbf{e}_r + \frac{1}{r}\frac{\partial p}{\partial \theta}\mathbf{e}_\theta + \frac{\partial p}{\partial z}\mathbf{e}_z, \quad \nabla \cdot \mathbf{u} = \frac{1}{r}\frac{\partial}{\partial r}(ru) + \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{\partial w}{\partial z},$$

$$\mathbf{K} = \begin{pmatrix} \frac{\partial u}{\partial r} & \frac{1}{r}\frac{\partial u}{\partial \theta} - \frac{v}{r} & \frac{\partial u}{\partial z} \\ \frac{\partial v}{\partial r} & \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{u}{r} & \frac{\partial v}{\partial z} \\ \frac{\partial w}{\partial r} & \frac{1}{r}\frac{\partial w}{\partial \theta} & \frac{\partial w}{\partial z} \end{pmatrix}$$

$$\nabla \cdot \boldsymbol{\sigma} = \begin{pmatrix} \frac{1}{r}\frac{\partial}{\partial r}(r\sigma_{rr}) + \frac{1}{r}\frac{\partial \sigma_{\theta r}}{\partial \theta} + \frac{\partial \sigma_{zr}}{\partial z} - \frac{\sigma_{\theta\theta}}{r} \\ \frac{1}{r^2}\frac{\partial}{\partial r}(r^2\sigma_{r\theta}) + \frac{1}{r}\frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{\partial \sigma_{z\theta}}{\partial z} + \frac{\sigma_{\theta r} - \sigma_{r\theta}}{r} \\ \frac{1}{r}\frac{\partial}{\partial r}(r\sigma_{rz}) + \frac{1}{r}\frac{\partial \sigma_{\theta z}}{\partial \theta} + \frac{\partial \sigma_{zz}}{\partial z} \end{pmatrix}$$

## Spherical Polar Coordinates

$$\mathbf{u} = u\mathbf{e}_r + v\mathbf{e}_\theta + w\mathbf{e}_\phi$$

$$\nabla p = \frac{\partial p}{\partial r}\mathbf{e}_r + \frac{1}{r}\frac{\partial p}{\partial \theta}\mathbf{e}_\theta + \frac{1}{r\sin\theta}\frac{\partial p}{\partial \phi}\mathbf{e}_\phi,$$

$$\nabla \cdot \mathbf{u} = \frac{1}{r^2}\frac{\partial}{\partial r}(r^2u) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(v\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial w}{\partial \phi},$$

$$\mathbf{K} = \begin{pmatrix} \frac{\partial u}{\partial r} & \frac{1}{r}\frac{\partial u}{\partial \theta} - \frac{v}{r} & \frac{1}{r\sin\theta}\frac{\partial u}{\partial \phi} - \frac{w}{r} \\ \frac{\partial v}{\partial r} & \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{u}{r} & \frac{1}{r\sin\theta}\frac{\partial v}{\partial \phi} - \frac{w}{r}\cot\theta \\ \frac{\partial w}{\partial r} & \frac{1}{r}\frac{\partial w}{\partial \theta} & \frac{1}{r\sin\theta}\frac{\partial w}{\partial \phi} + \frac{u}{r} + \frac{v}{r}\cot\theta \end{pmatrix}$$

$$\nabla \cdot \boldsymbol{\sigma} = \begin{pmatrix} \frac{1}{r^2}\frac{\partial}{\partial r}(r^2\sigma_{rr}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta r}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi r}}{\partial \phi} - \frac{\sigma_{\theta\theta} + \sigma_{\phi\phi}}{r} \\ -\frac{1}{r^3}\frac{\partial}{\partial r}(r^3\sigma_{r\theta}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta\theta}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi\theta}}{\partial \phi} + \frac{\sigma_{\theta r} - \sigma_{r\theta} - \sigma_{\phi\phi}\cot\theta}{r} \\ \frac{1}{r^3}\frac{\partial}{\partial r}(r^3\sigma_{r\phi}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta\phi}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi\phi}}{\partial \phi} + \frac{\sigma_{\phi r} - \sigma_{r\phi} + \sigma_{\phi\theta}\cot\theta}{r} \end{pmatrix}$$