

## MATH445001

This question paper consists of 8 printed pages, each of which is identified by the reference **MATH4450**.

Only approved basic scientific calculators may be used.

## © UNIVERSITY OF LEEDS

Examination for the Module MATH4450

(May/June 2002)

**Polymeric Fluids**

Time allowed: **3 hours**

Answer FIVE of the SEVEN questions.

All questions carry equal marks.

1. In the power-law fluid model the shear stress,  $\sigma$  is equal to  $\sigma = K|\dot{\gamma}|^{n-1}\dot{\gamma}$ , where  $K$  and  $n$  are positive constants.
  - (a) Explain what is meant by the terms *shear thinning* and *shear thickening* and state the range of values of  $n$  for which the power law fluid is shear-thinning or shear-thickening.
  - (b) A power-law fluid is driven along a cylindrical pipe of radius  $a$  by a pressure gradient  $\frac{\partial p}{\partial z} = -G$ . Show that the shear stress  $\sigma$  is given in terms of the shear-rate  $\dot{\gamma}$  by

$$\sigma = -\frac{1}{2}Gr.$$

Find the form of the fluid velocity,  $w$  and sketch a graph showing  $w(r)$  for (a)  $n = 0.5$ , (b)  $n = 1$  and (c)  $n = 2$ . Explain the differences in the velocity profiles.

- (c) Calculate the volume flux,  $Q = 2\pi \int_0^a r w dr$  down the pipe. A Newtonian fluid of viscosity  $\mu$  and a power-law fluid of index  $n = 0.5$  have the same volume flow rate down a pipe of radius  $a$  when a pressure gradient  $G$  is applied. Find the increase in the volume flow -rate of each fluid if:
  - (i) the pressure gradient is doubled from  $G$  to  $2G$ ,
  - (ii) the pipe is replaced by a pipe of radius  $2a$ .

Explain why the volume flow rate of the shear-thinning fluid is now larger in both cases.

2. (a) Write down the equations of mass and momentum conservation for an incompressible fluid with pressure,  $p$ , density,  $\rho$ , extra stress,  $\boldsymbol{\sigma}$ , and velocity,  $\mathbf{u}$ , that is subject to a gravitational acceleration  $\mathbf{g}$ . Under what circumstances can fluid inertia be neglected and how does this simplify these equations?
- (b) Using the appropriate formulae for cylindrical polar coordinates write down the velocity gradient for a flow in which the fluid velocity is given in cylindrical polar coordinates  $(r, \theta, z)$  by  $\mathbf{u} = (0, v(r), 0)$ . Show that the  $r\theta$  component of the strain-rate tensor,  $\mathbf{E}$ ,

$$E_{r\theta} = \frac{1}{2}\dot{\gamma} = \frac{r}{2} \frac{\partial}{\partial r} \left( \frac{v}{r} \right),$$

where  $\dot{\gamma}$  is the local shear-rate. Define the shear viscosity,  $\mu(\dot{\gamma})$ , and first and second normal stress differences,  $N_1(\dot{\gamma})$  and  $N_2(\dot{\gamma})$ , in terms of the components of the extra stress tensor  $\boldsymbol{\sigma}$ .

- (c) A vertical rod of radius  $a$  rotates at an angular velocity  $\Omega$  in a polymeric fluid in which

$$\mu(\dot{\gamma}) = \mu_0, \quad N_1(\dot{\gamma}) = A\dot{\gamma}^2, \quad N_2(\dot{\gamma}) = 0,$$

where  $\mu_0$  and  $A$  are both positive constants. Write down the components of the momentum equation on the assumption that fluid inertia is negligible, and show that this leads to the following equations

$$\begin{aligned} \frac{\mu_0}{r^2} \frac{\partial}{\partial r} (r^2 \dot{\gamma}) &= 0, \\ \frac{\partial}{\partial r} (-p + \sigma_{zz}) &= \frac{A}{r} \dot{\gamma}^2, \\ \frac{\partial}{\partial z} (-p + \sigma_{zz}) &= \rho g. \end{aligned}$$

Hence find the fluid velocity  $v(r)$  and show that

$$\dot{\gamma} = -\frac{2\Omega a^2}{r^2}.$$

- (d) If the top surface is open to the atmosphere, show that the position of this surface is given by

$$h(r) = h_\infty + \frac{A\Omega^2 a^2}{\rho g r^4},$$

where  $h_\infty$  is the height for  $r \rightarrow \infty$ .

3. The extra stress  $\boldsymbol{\sigma}$  in the linear Maxwell model is related to the strain-rate by

$$\tau \frac{\partial \boldsymbol{\sigma}}{\partial t} + \boldsymbol{\sigma} = 2\mu \mathbf{E}(t).$$

Show that this may be written in the form

$$\boldsymbol{\sigma} = 2 \int_{-\infty}^t G(t-t') \mathbf{E}(t') dt',$$

for some suitable choice for the relaxation modulus  $G(t)$ . Show that

$$\int_0^\infty G(t)dt = \mu.$$

Find the shear stress  $\sigma_{xy}(t)$  generated by the fluid velocity  $\mathbf{u} = (\dot{\gamma}y, 0, 0)$  in the following cases:

$$\begin{aligned} \text{(a)} \quad \dot{\gamma} &= \begin{cases} k & t < 0, \\ 0 & t \geq 0. \end{cases} \\ \text{(b)} \quad \dot{\gamma} &= \begin{cases} k & -T \leq t < 0, \\ -k & 0 \leq t \leq T, \\ 0 & |t| > T. \end{cases} \end{aligned}$$

For each case sketch graphs of  $\sigma_{xy}$  and  $\dot{\gamma}$  as functions of time. For case (c) show that there must be a time  $t_0$  in the interval  $0 < t_0 < T$  at which  $\sigma_{xy} = 0$ . Find the value of  $t_0$ .

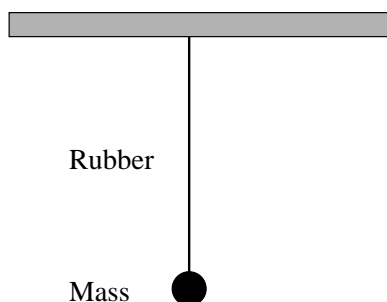
4. The expression for the total stress in a rubber is

$$\boldsymbol{\tau} = G\mathbf{F} \cdot \mathbf{F}^T - \beta\mathbf{I}.$$

- (a) What is the deformation gradient,  $\mathbf{F}$ , and stress,  $\boldsymbol{\tau}$ , for uniaxial extension by a ratio  $\lambda$  in the  $z$ -direction? A piece of rubber, of initial cross sectional area  $A_0$  is stretched by a ratio  $\lambda$ . If the sides of the rubber are exposed to the atmosphere, so that  $\tau_{xx} = \tau_{yy} = -p_{atm}$ , show that the force required to achieve the stretch is

$$f = GA_0 \left( \lambda - \frac{1}{\lambda^2} \right).$$

- (b) A mass  $m$  is suspended from a piece of rubber of initial length  $l_0$  and cross sectional area  $A_0$ , as shown in the diagram.



- (i) What is the relationship between the stretch  $\lambda$ , the length of the rubber,  $l$ , and the initial length,  $l_0$ ?
- (ii) By balancing the forces on the mass, obtain a relation between the mass  $m$  and the equilibrium stretch of the rubber  $\lambda_{eq}$ .

- (iii) What is the change in  $\lambda$  for a small downward displacement  $x$  from the equilibrium position? By considering the forces on the mass after such a displacement, show that

$$m \frac{d^2 x}{dt^2} = -\frac{GA_0}{l_0} \left( 1 + \frac{2}{\lambda_{eq}^3} \right) x.$$

- (iv) Hence show that the time period for small vertical oscillations is

$$T_v = 2\pi \left( \frac{l_0}{g} \frac{\lambda_{eq}^4 - \lambda_{eq}}{\lambda_{eq}^3 + 2} \right)^{\frac{1}{2}},$$

where  $g$  is the acceleration due to gravity.

5. The Langevin equation for a particle in a quadratic potential  $U = \frac{1}{2}kx^2$  is

$$\zeta \frac{dx}{dt} = -kx + f(t),$$

where  $\langle f(t) f(t') \rangle = 2k_B T \zeta \delta(t - t')$ .

- (a) Show that the solution of this equation, subject to initial condition  $x(0) = 0$ , is

$$x(t) = \frac{1}{\zeta} \int_0^t dt' f(t') \exp\left(-\frac{t' - t}{\tau}\right),$$

where  $\tau = \frac{\zeta}{k}$ .

- (b) Hence show that

$$\langle x(t)^2 \rangle = \frac{k_B T}{k} \left( 1 - \exp\left(-\frac{2t}{\tau}\right) \right).$$

- (c)

- (i) Obtain the limiting form of  $\langle x(t)^2 \rangle$  for  $t \ll \tau$  and compare your result with free-particle diffusion (where  $\langle x(t)^2 \rangle = 2Dt$ ).
- (ii) Obtain the limiting form of  $\langle x(t)^2 \rangle$  for  $t \gg \tau$ . In this limit, show that the average energy  $\langle U \rangle$  approaches  $\frac{1}{2}k_B T$ .

6. The Rouse equation for a polymer chain comprising beads with friction constant  $\zeta$  connected with springs of spring constant  $k$  is

$$\zeta \left( \frac{\partial \mathbf{r}_s}{\partial t} - \mathbf{v}(\mathbf{r}_s) \right) = k \frac{\partial^2 \mathbf{r}_s}{\partial s^2} + \mathbf{f}_s, \quad s = 0..N,$$

with boundary conditions

$$\left. \frac{\partial \mathbf{r}_s}{\partial s} \right|_{s=0} = 0 \quad \text{and} \quad \left. \frac{\partial \mathbf{r}_s}{\partial s} \right|_{s=N} = 0.$$

- (a) In terms of the forces acting on a bead, briefly discuss the origin of the term,  $\frac{\partial^2 \mathbf{r}_s}{\partial s^2}$ .

- (b) Ignoring the terms due to velocity,  $\mathbf{v}(\mathbf{r}_s)$ , and random force,  $\mathbf{f}_s$ , show that the relaxation time of the  $p$ th normal mode,  $\mathbf{r}_s = \mathbf{X}_p \cos\left(\frac{\pi p s}{N}\right)$ , is

$$\tau_p = \frac{\tau_1}{p^2},$$

where  $\tau_1 = \frac{N^2 \zeta}{\pi^2 k}$ .

- (c) Given that this leads to a time-dependent modulus of form

$$G(t) = G_0 \sum_{p=1}^{\infty} \exp\left(-\frac{p^2 t}{\tau_1}\right),$$

use  $G^* = G' + iG'' = \int_0^{\infty} i\omega G(s) \exp(-i\omega s) ds$  to show that

$$\begin{aligned} G' &= G_0 \sum_{p=1}^{\infty} \frac{\omega^2 \tau_1^2}{p^4 + \omega^2 \tau_1^2}, \\ G'' &= G_0 \sum_{p=1}^{\infty} \frac{p^2 \omega \tau_1}{p^4 + \omega^2 \tau_1^2}, \end{aligned}$$

and obtain approximations of the form  $G'' = c\omega^\alpha$  for  $\omega\tau_1 \ll 1$  and (by approximating the sum as an integral) for  $\omega\tau_1 \gg 1$ . Hence sketch a graph of  $\log G''$  versus  $\log \omega$ .

You may use the results:

$$\begin{aligned} \sum_{p=1}^{\infty} p^{-2} &= \frac{\pi^2}{6}, \\ \int_0^{\infty} \frac{x^2}{1+x^4} dx &= \frac{\pi}{2\sqrt{2}}. \end{aligned}$$

7. The stress in the upper convected Maxwell model is given by

$$\boldsymbol{\tau} = -\beta \mathbf{I} + G \mathbf{A},$$

where the second rank tensor  $\mathbf{A}$  satisfies

$$\frac{D\mathbf{A}}{Dt} = \mathbf{K} \cdot \mathbf{A} + \mathbf{A} \cdot \mathbf{K}^T - \frac{1}{\tau} (\mathbf{A} - \mathbf{I}),$$

and  $K_{ij} = \frac{\partial u_i}{\partial x_j}$  is the velocity gradient.

Fluid is placed in the gap between two plates of surface area  $S$  located at  $z = \pm h$ . Each plate is coated with a lubricant so that the fluid can slip at the plate surfaces, so that the fluid velocity between the plates is of the form

$$\mathbf{u} = (E(t)x, E(t)y, -2E(t)z).$$

Show that

$$E(t) = -\frac{1}{2h} \frac{dh}{dt}.$$

Find  $E(t)$  if the plates are squeezed together so that

$$h(t) = \begin{cases} h_0 e^{-\frac{2t}{\tau}} & 0 \leq t \leq \tau, \\ h_0 e^{-2} & t > \tau. \end{cases}$$

The fluid is at equilibrium at  $t = 0$ , so that  $\mathbf{A} = \mathbf{I}$ . Deduce that for  $t > 0$  the only non-zero components of the  $\mathbf{A}$  are  $A_{xx}$ ,  $A_{yy}$  and  $A_{zz}$  and that  $A_{xx} = A_{yy}$ . Find  $\mathbf{A}(t)$  for  $t > 0$ . If the edges of the plates are open to the atmosphere so that  $\tau_{xx} = \tau_{yy} = -p_{\text{atm}}$ , show that the net force exerted by the fluid on the plates,

$$F = GS(A_{xx} - A_{zz})$$

Find  $F(t)$  and explain why  $F$  is non-zero for  $t > \tau$ ?

## Formulae Sheet

### Cartesian coordinates

pressure,  $p$ , velocity,  $\mathbf{u} = u\mathbf{e}_x + v\mathbf{e}_y + w\mathbf{e}_z$ , velocity gradient,  $\mathbf{K}$  with  $K_{ij} = \frac{\partial u_i}{\partial x_j}$

$$\begin{aligned}\nabla p &= \frac{\partial p}{\partial x}\mathbf{e}_x + \frac{\partial p}{\partial y}\mathbf{e}_y + \frac{\partial p}{\partial z}\mathbf{e}_z, & \nabla \cdot \mathbf{u} &= \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z}, \\ \mathbf{K} &= \begin{pmatrix} \frac{\partial u}{\partial x} & \frac{\partial u}{\partial y} & \frac{\partial u}{\partial z} \\ \frac{\partial v}{\partial x} & \frac{\partial v}{\partial y} & \frac{\partial v}{\partial z} \\ \frac{\partial w}{\partial x} & \frac{\partial w}{\partial y} & \frac{\partial w}{\partial z} \end{pmatrix} & \nabla \cdot \boldsymbol{\sigma} &= \begin{pmatrix} \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{yx}}{\partial y} + \frac{\partial \sigma_{zx}}{\partial z} \\ \frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{zy}}{\partial z} \\ \frac{\partial \sigma_{xz}}{\partial x} + \frac{\partial \sigma_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} \end{pmatrix}\end{aligned}$$

### Cylindrical Polar Coordinates

velocity,  $\mathbf{u} = u\mathbf{e}_r + v\mathbf{e}_\theta + w\mathbf{e}_z$ .

$$\begin{aligned}\nabla p &= \frac{\partial p}{\partial r}\mathbf{e}_r + \frac{1}{r}\frac{\partial p}{\partial \theta}\mathbf{e}_\theta + \frac{\partial p}{\partial z}\mathbf{e}_z, & \nabla \cdot \mathbf{u} &= \frac{1}{r}\frac{\partial}{\partial r}(ru) + \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{\partial w}{\partial z}, \\ \mathbf{K} &= \begin{pmatrix} \frac{\partial u}{\partial r} & \frac{1}{r}\frac{\partial u}{\partial \theta} - \frac{v}{r} & \frac{\partial u}{\partial z} \\ \frac{\partial v}{\partial r} & \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{u}{r} & \frac{\partial v}{\partial z} \\ \frac{\partial w}{\partial r} & \frac{1}{r}\frac{\partial w}{\partial \theta} & \frac{\partial w}{\partial z} \end{pmatrix} \\ \nabla \cdot \boldsymbol{\sigma} &= \begin{pmatrix} \frac{1}{r}\frac{\partial}{\partial r}(r\sigma_{rr}) + \frac{1}{r}\frac{\partial \sigma_{\theta r}}{\partial \theta} + \frac{\partial \sigma_{zr}}{\partial z} - \frac{\sigma_{\theta\theta}}{r} \\ \frac{1}{r^2}\frac{\partial}{\partial r}(r^2\sigma_{r\theta}) + \frac{1}{r}\frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{\partial \sigma_{z\theta}}{\partial z} + \frac{\sigma_{\theta r} - \sigma_{r\theta}}{r} \\ \frac{1}{r}\frac{\partial}{\partial r}(r\sigma_{rz}) + \frac{1}{r}\frac{\partial \sigma_{\theta z}}{\partial \theta} + \frac{\partial \sigma_{zz}}{\partial z} \end{pmatrix}\end{aligned}$$

## Spherical Polar Coordinates

$$\mathbf{u} = u\mathbf{e}_r + v\mathbf{e}_\theta + w\mathbf{e}_\phi$$

$$\nabla p = \frac{\partial p}{\partial r}\mathbf{e}_r + \frac{1}{r}\frac{\partial p}{\partial \theta}\mathbf{e}_\theta + \frac{1}{r\sin\theta}\frac{\partial p}{\partial \phi}\mathbf{e}_\phi,$$

$$\nabla \cdot \mathbf{u} = \frac{1}{r^2}\frac{\partial}{\partial r}(r^2u) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(v\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial w}{\partial \phi},$$

$$\mathbf{K} = \begin{pmatrix} \frac{\partial u}{\partial r} & \frac{1}{r}\frac{\partial u}{\partial \theta} - \frac{v}{r} & \frac{1}{r\sin\theta}\frac{\partial u}{\partial \phi} - \frac{w}{r} \\ \frac{\partial v}{\partial r} & \frac{1}{r}\frac{\partial v}{\partial \theta} + \frac{u}{r} & \frac{1}{r\sin\theta}\frac{\partial v}{\partial \phi} - \frac{w}{r}\cot\theta \\ \frac{\partial w}{\partial r} & \frac{1}{r}\frac{\partial w}{\partial \theta} & \frac{1}{r\sin\theta}\frac{\partial w}{\partial \phi} + \frac{w}{r} + \frac{v}{r}\cot\theta \end{pmatrix}$$

$$\nabla \cdot \boldsymbol{\sigma} = \begin{pmatrix} \frac{1}{r^2}\frac{\partial}{\partial r}(r^2\sigma_{rr}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta r}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi r}}{\partial \phi} - \frac{\sigma_{\theta\theta} + \sigma_{\phi\phi}}{r} \\ \frac{1}{r^3}\frac{\partial}{\partial r}(r^3\sigma_{r\theta}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta\theta}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi\theta}}{\partial \phi} + \frac{\sigma_{\theta r} - \sigma_{r\theta} - \sigma_{\phi\phi}\cot\theta}{r} \\ \frac{1}{r^3}\frac{\partial}{\partial r}(r^3\sigma_{r\phi}) + \frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(\sigma_{\theta\phi}\sin\theta) + \frac{1}{r\sin\theta}\frac{\partial \sigma_{\phi\phi}}{\partial \phi} + \frac{\sigma_{\phi r} - \sigma_{r\phi} + \sigma_{\phi\theta}\cot\theta}{r} \end{pmatrix}$$