

MATHEMATICAL TRIPOS      Part III

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Thursday 9 June, 2005    9 to 11

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PAPER 82

SEISMIC WAVES

*Attempt up to **FOUR** questions.*

*Full marks will be awarded for the equivalent of complete answers to **two** questions.*

*There are **FOUR** questions in total.*

*The questions carry equal weight.*

**STATIONERY REQUIREMENTS**

*Cover sheet*

*Treasury tag*

*Script paper*

**SPECIAL REQUIREMENTS**

*None*

<p><b>You may not start to read the questions printed on the subsequent pages until instructed to do so by the Invigilator.</b></p>
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1 (a) From the equations for 1-dimensional elastic waves

$$\rho \frac{\partial v}{\partial t} = \frac{\partial \sigma}{\partial x}, \quad \frac{\partial \sigma}{\partial t} = \mu \frac{\partial v}{\partial x}, \quad \text{with} \quad \beta = \sqrt{\frac{\mu}{\rho}},$$

show that in uniform media there are two independent solutions  $(v_+, \sigma_+)$  and  $(v_-, \sigma_-)$  satisfying

$$\sigma_+ = -\rho\beta v_+, \quad \sigma_- = \rho\beta v_-,$$

with energy fluxes  $S = -v\sigma$  in the positive and negative  $x$ -directions respectively.

(b) Convert the above differential equations for continuous media into the following equations for  $\phi_+$  and  $\phi_-$  such that

$$v = \frac{1}{\sqrt{\rho\beta}} (\phi_+ + \phi_-), \quad \sigma = -\sqrt{\rho\beta} (\phi_+ - \phi_-):$$

$$\begin{aligned} \frac{\partial \phi_+}{\partial x} + \frac{1}{\beta} \frac{\partial \phi_+}{\partial t} &= \frac{1}{2} \left\{ \frac{\partial}{\partial x} \ln(\rho\beta) \right\} \phi_-, \\ \frac{\partial \phi_-}{\partial x} - \frac{1}{\beta} \frac{\partial \phi_-}{\partial t} &= \frac{1}{2} \left\{ \frac{\partial}{\partial x} \ln(\rho\beta) \right\} \phi_+. \end{aligned}$$

(c) For time-harmonic waves with angular frequency  $\omega$  and for a continuously differentiable monotonic variation in seismic impedance  $\rho\beta$  between  $x_a$  and  $x_b$  ( $> x_a$ ) such that

$$|\omega| \int_{x_a}^{x_b} \frac{dx}{\beta} \ll \text{both } 1 \text{ and } \frac{1}{2} \left| \ln \left( \frac{\rho_b \beta_b}{\rho_a \beta_a} \right) \right|,$$

where  $\rho_a \beta_a$  and  $\rho_b \beta_b$  are the impedances at  $x_a$  and  $x_b$ , use the differential equations for  $\phi_+$  and  $\phi_-$  to find reflection and transmission coefficients  $R_{aa}$ ,  $T_{ab}$ ,  $T_{ba}$ ,  $R_{bb}$  depending on only  $\rho_a \beta_a$  and  $\rho_b \beta_b$  such that to zeroth-order in frequency

$$\begin{pmatrix} \phi_-(x_a) \\ \phi_+(x_b) \end{pmatrix} = \begin{pmatrix} R_{aa} & T_{ab} \\ T_{ba} & R_{bb} \end{pmatrix} \begin{pmatrix} \phi_+(x_a) \\ \phi_-(x_b) \end{pmatrix}.$$

(d) Relate your answer to part (c) to corresponding expressions for reflection and transmission at a discontinuity in the medium, and show that in this zeroth-order in frequency limit the total time-averaged energy flux  $\frac{1}{2} [|\phi_-(x_a)|^2 + |\phi_+(x_b)|^2]$  out of the region is the same as the total time-averaged energy flux  $\frac{1}{2} [|\phi_+(x_a)|^2 + |\phi_-(x_b)|^2]$  into the region. Use the differential equations for  $\phi_+$  and  $\phi_-$  to demonstrate that for time-harmonic waves

$$\frac{d}{dx} [|\phi_+(x)|^2 - |\phi_-(x)|^2] = 0$$

and, hence, that this equality of energy fluxes into and out of the region is satisfied exactly at all frequencies.

**2** **Either, (a)** Describe, defining all required terms, all the steps in deriving the transport equation for the leading-order P-wave wavefield discontinuity in the form

$$0 = \frac{\partial}{\partial x_q} \left( \rho \alpha \left( a^{[k]} \right)^2 n_q \right)$$

for a continuous isotropic medium, where  $a^{[k]}$  is the amplitude of the discontinuity at the wavefront and  $k \geq 2$  denotes the order of the time derivative of displacement involved.

**Or (b)** For the case of a uniform isotropic superficial layer of thickness  $h$  over a uniform isotropic halfspace, derive the dispersion relationship for Love waves

$$\tan \left( |\omega| h \sqrt{\frac{1}{\beta_0^2} - \frac{1}{c_L^2}} \right) = \frac{\mu \sqrt{\frac{1}{c_L^2} - \frac{1}{\beta^2}}}{\mu_0 \sqrt{\frac{1}{\beta_0^2} - \frac{1}{c_L^2}}}$$

using both of the following two approaches:

- (i) direct solution of the equations for SH waves, and
- (ii) derivation of the condition for constructive interference of SH waves multiply reflected in the superficial layer, including derivation of the reflection coefficients involved.

Here  $\omega$  is the angular frequency,  $c_L$  is the Love wave speed,  $\beta_0$  and  $\beta (> \beta_0)$  are the S wave speeds in the layer and the halfspace, and  $\mu_0$  and  $\mu$  are the corresponding shear moduli.

- (iii) Explain the significance of the frequencies where  $c_L = \beta$ .

**[Do not attempt both parts of this question.]**

**3** In a bounded perfectly elastic domain  $\mathcal{D}$ , with boundary  $\partial\mathcal{D}$ , density  $\rho(\mathbf{x})$  and stiffness tensor  $c_{ijpq}(\mathbf{x})$ , consider the Fourier components  $\widehat{u}_i(\mathbf{x}, \omega) e^{-i\omega t}$  for real-valued frequencies  $\omega$  of a real-valued displacement field  $u_i(\mathbf{x}, t)$  associated with real-valued body forces  $f_i(\mathbf{x}, t)$ , with corresponding Fourier components  $\widehat{f}_i(\mathbf{x}, \omega) e^{-i\omega t}$ . Each  $\widehat{u}_i(\mathbf{x}, \omega)$  satisfies

$$0 = \rho\omega^2\widehat{u}_i + \frac{\partial\widehat{\sigma}_{ij}}{\partial x_j} + \widehat{f}_i \quad \text{where} \quad \widehat{\sigma}_{ij}(\mathbf{x}, \omega) = c_{ijpq}\frac{\partial}{\partial x_p}\widehat{u}_q(\mathbf{x}, \omega).$$

Also note that  $\widehat{u}_i(\mathbf{x}, -\omega) = \widehat{u}_i(\mathbf{x}, \omega)^*$  and  $\widehat{f}_i(\mathbf{x}, -\omega) = \widehat{f}_i(\mathbf{x}, \omega)^*$ .

(a) For any two such wavefields  $\widehat{u}_i^a(\mathbf{x}, \omega_a)$  and  $\widehat{u}_i^b(\mathbf{x}, \omega_b)$  establish that

$$\int_D \left\{ -\left(\rho\omega_a^2\widehat{u}_i^a + \widehat{f}_i^a\right)\widehat{u}_i^b + \widehat{u}_i^a\left(\rho\omega_b^2\widehat{u}_i^b + \widehat{f}_i^b\right) \right\} dV = \int_{\partial\mathcal{D}} \left\{ (\widehat{\sigma}_{ij}^a n_j)\widehat{u}_i^b - \widehat{u}_i^a(\widehat{\sigma}_{ij}^b n_j) \right\} dS.$$

(b) Use this expression to prove that for any single wavefield  $\widehat{u}_i(\mathbf{x}, \omega)$

$$\int_D \left\{ \widehat{f}_i^* \widehat{v}_i + \widehat{v}_i^* \widehat{f}_i \right\} dV = \int_{\partial\mathcal{D}} \left\{ -(\widehat{\sigma}_{ij}^* n_j)\widehat{v}_i - \widehat{v}_i^*(\widehat{\sigma}_{ij} n_j) \right\} dS$$

where  $\widehat{v}_i(\mathbf{x}, \omega) e^{-i\omega t} = -i\omega\widehat{u}_i(\mathbf{x}, \omega) e^{-i\omega t}$  is the corresponding Fourier component of the velocity  $v_i(\mathbf{x}, t) = \frac{\partial}{\partial t}u_i(\mathbf{x}, t)$ . Interpret this result in terms of the time-averaged work done by the combined body forces  $\widehat{f}_i(\mathbf{x}, \omega) e^{-i\omega t} + \widehat{f}_i(\mathbf{x}, -\omega) e^{i\omega t}$  and the corresponding outward flow of energy at the boundary  $\partial\mathcal{D}$ .

(c) For wavefields  $\widehat{u}_i^a(\mathbf{x}, \omega_a)$  and  $\widehat{u}_i^b(\mathbf{x}, \omega_b)$  for which  $\widehat{f}_i^a(\mathbf{x}, \omega_a) = 0$  and  $\widehat{f}_i^b(\mathbf{x}, \omega_b) = 0$  establish that

$$\int_D \rho(\widehat{u}_i^a)^* \widehat{u}_i^b dV = 0$$

if  $\omega_a^2 \neq \omega_b^2$  and both wavefields satisfy traction-free boundary conditions on  $\partial\mathcal{D}$ . From this deduce that there are at most a countably infinite number of frequencies  $\omega$  such that  $\widehat{u}_i(\mathbf{x}, \omega)$  can be non-zero when there are no body or boundary forces.

(d) Hence, prove that for all other frequencies the solutions to

$$0 = \rho\omega^2\widehat{u}_i + \frac{\partial\widehat{\sigma}_{ij}}{\partial x_j} + \widehat{f}_i$$

with traction boundary conditions on  $\partial\mathcal{D}$  are unique, and that for traction boundary conditions the complete wavefield  $u_i(\mathbf{x}, t)$  becomes unique when initial conditions  $u_i(\mathbf{x}, 0) = 0$  and  $v_i(\mathbf{x}, 0) = 0$  are applied everywhere in the domain  $\mathcal{D}$ .

4 In a uniform isotropic medium consider P-SV waves propagating in the  $(x, z)$  plane with  $x$  and  $t$  dependence of the form  $e^{i(kx - \omega t)}$  with  $\omega$  real and positive, and  $k$  also real and such that  $|k| < \frac{\omega}{\alpha}$  ( $< \frac{\omega}{\beta}$ ), so that both

$$k_\alpha = \sqrt{\frac{\omega^2}{\alpha^2} - k^2} \quad \text{and} \quad k_\beta = \sqrt{\frac{\omega^2}{\beta^2} - k^2}$$

are also real-valued.

(a) For waves involving propagation in the positive  $z$ -direction, with P and S wave potentials of the form

$$\phi_+ = A_+ e^{i(kx + k_\alpha z - \omega t)}, \quad \psi_+ = B_+ e^{i(kx + k_\beta z - \omega t)},$$

determine the matrix  $Z_+$  such that

$$\begin{pmatrix} \sigma_{xz} \\ \sigma_{zz} \end{pmatrix} = -Z_+ \begin{pmatrix} v_x \\ v_z \end{pmatrix},$$

and hence prove that the time-averaged energy flux in the  $z$ -direction

$$\frac{1}{4} \begin{pmatrix} v_x \\ v_z \end{pmatrix}^\dagger (Z_+ + Z_+^\dagger) \begin{pmatrix} v_x \\ v_z \end{pmatrix} \quad (= \frac{1}{2} \text{Re} \{-v_x^* \sigma_{xz} - v_z^* \sigma_{zz}\})$$

$$\text{is} \quad \frac{\rho\omega}{2(k^2 + k_\alpha k_\beta)} (k_\alpha |v_x|^2 + k_\beta |v_z|^2) (> 0),$$

where  $\dagger$  denotes the transpose of the complex conjugate.

(b) Similarly, for waves involving propagation in the negative  $z$ -direction, with P and S wave potentials of the form

$$\phi_- = A_- e^{i(kx - k_\alpha z - \omega t)}, \quad \psi_- = B_- e^{i(kx - k_\beta z - \omega t)},$$

determine the corresponding matrix  $Z_-$ , establishing that  $Z_- = -Z_+^\dagger$ , and prove that the time-averaged energy flux in the  $z$ -direction is

$$\frac{\rho\omega}{2(k^2 + k_\alpha k_\beta)} (-k_\alpha |v_x|^2 - k_\beta |v_z|^2) (< 0).$$

(c) For a mixture of waves involving propagation in both the positive and negative  $z$ -directions, with

$$\begin{pmatrix} v_x \\ v_z \end{pmatrix} = \begin{pmatrix} v_x^+ \\ v_z^+ \end{pmatrix} + \begin{pmatrix} v_x^- \\ v_z^- \end{pmatrix} \quad \text{and} \quad \begin{pmatrix} \sigma_{xz} \\ \sigma_{zz} \end{pmatrix} = -Z_+ \begin{pmatrix} v_x^+ \\ v_z^+ \end{pmatrix} - Z_- \begin{pmatrix} v_x^- \\ v_z^- \end{pmatrix},$$

explain how  $v_x^+$ ,  $v_z^+$ ,  $v_x^-$ ,  $v_z^-$  can be determined from  $v_x$ ,  $v_z$ ,  $\sigma_{xz}$ ,  $\sigma_{zz}$  and obtain an explicit expression for  $(Z_+ - Z_-)^{-1}$ . Establish that in this case the time-averaged energy flux in the  $z$ -direction is

$$\frac{\rho\omega}{2(k^2 + k_\alpha k_\beta)} (k_\alpha [|v_x^+|^2 - |v_x^-|^2] + k_\beta [|v_z^+|^2 - |v_z^-|^2]),$$

and that this expression can be rewritten as

$$\frac{\rho\omega^3}{2} (k_\alpha [|\phi_+|^2 - |\phi_-|^2] + k_\beta [|\psi_+|^2 - |\psi_-|^2]).$$

**END OF PAPER**