

Q2 (a) Write the differential equation describing the dynamics of the system shown

Fig.1 and find  $\frac{x_2(s)}{F(s)}$

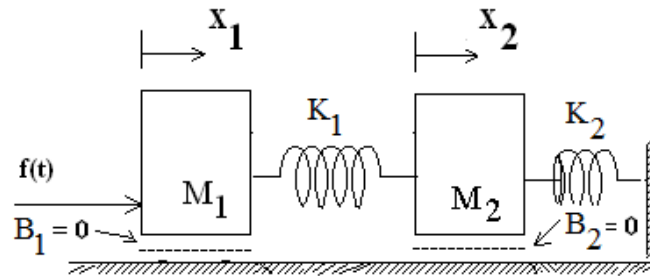
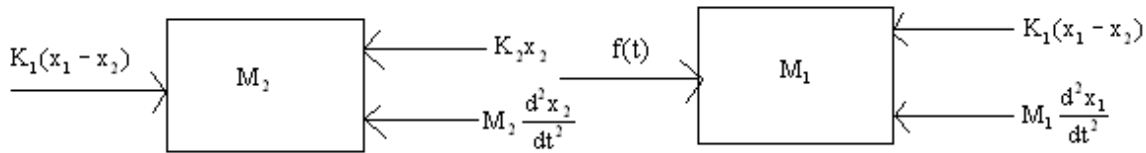


Fig.1

Answer

Free body diagrams for mass  $M_1$  and  $M_2$  are



For  $M_2$

For  $M_1$

$$F(t) = M_1 \frac{d^2 x_1}{dt^2} + K_1(x_1 - x_2) \quad (1)$$

$$K_1(x_1 - x_2) = K_2 x_2 + M_2 \frac{d^2 x_2}{dt^2} \quad (2)$$

Take Laplace transform of eq. (1) & eq. (2) under initial conditions as zero.

$$F(s) = M_1 s^2 x_1(s) + K_1 x_1(s) - K_2 x_2(s) + M_2 s^2 x_2(s) \quad (3)$$

$$K_1 x_1(s) - K_1 x_2(s) = K_2 x_2(s) + M_2 s^2 x_2(s) \quad (4)$$

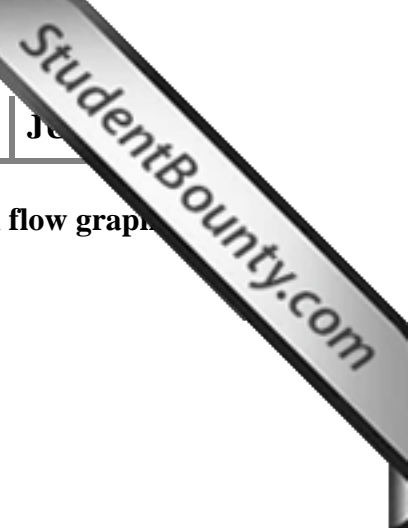
$$\text{Solving (3) \& (4) we get } x_1(s) = \frac{x_2(s)}{K_1} (s^2 M_2 + K_1 + K_2) \quad (5)$$

$$F(s) = \frac{x_2(s)}{K_1} (s^2 M_2 + K_1 + K_2) (s^2 M_1 + K_1) + K_1 x_2(s)$$

$$\text{or } \frac{x_2(s)}{f(s)} = \frac{K_1}{(s^2 M_2 + K_1 + K_2)(K_1 + s^2 M_1) - K_1^2}$$

Q2 (b) Obtain the F-I and F-V analogy of (a).

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Q3 (a) In the Fig.4, identify the set of state variables and draw the signal flow graph of the circuit.

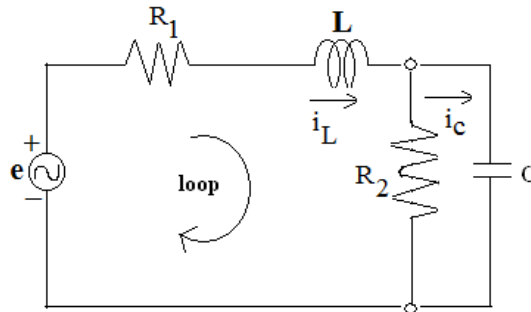


Fig.4

Also, determine transfer function from signal flow graph.

**Answer**

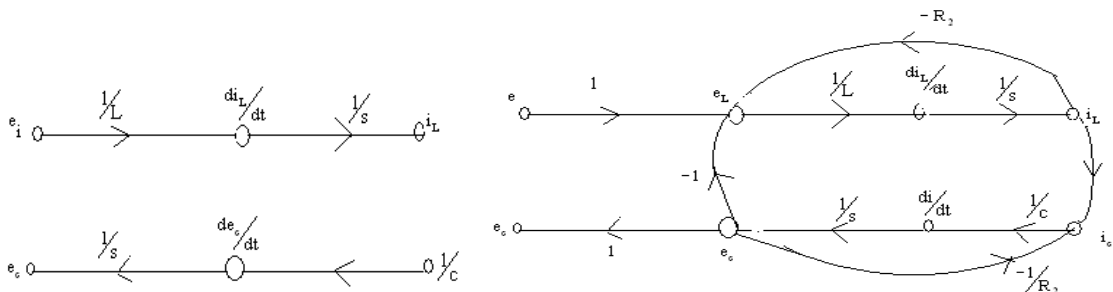
The Circuit of Fig.4 has two storage elements, so these shall be two state variables  $i_L$  and  $e_c$ .

The signal flow graph is conflicted by KCL equation at node and KVL equation round the loop. There are

$$v_L = \frac{e_c}{R_2} + i_c \text{ or } v_L = i_L \frac{e_c}{R_2} \text{ _____ (1)}$$

$$\text{and } e = R_1 i_L + e_L + e_c \text{ or } e_L = e - R_1 i_L - e_c \text{ _____ (2)}$$

The signal flow graph is drawn



(a)

(b)

**Signal flow graph**

From signal flow graph, the two state variable equations be written as

$$\frac{di_L}{dt} = \frac{1}{L} e_L = \frac{1}{L} (-e_c - R_1 i_L + e) = \frac{-R_1}{L} i_L - \frac{1}{L} e_c + \frac{1}{L} e \text{ _____ (3)}$$

$$\text{and } \frac{de_c}{dt} = \frac{1}{C} i_L = \frac{1}{C} (i_L + \frac{e_c}{R_2}) = \frac{1}{C} i_L - \frac{1}{R_2 C} e_c \text{ _____ (4)}$$

eq. (3) & (4) in the matrix form

$$\begin{bmatrix} \frac{di_L}{dt} \\ \frac{di_c}{dt} \end{bmatrix} = \begin{bmatrix} -\frac{R_1}{L} & \frac{1}{L} \\ \frac{1}{C} & \frac{1}{R_2} \end{bmatrix} \begin{bmatrix} i_L \\ i_c \end{bmatrix} + \begin{bmatrix} \frac{1}{L} \\ 0 \end{bmatrix} e$$

Forward path  $P_1 = \frac{1}{sL} \times \frac{1}{sC} = \frac{1}{s^2LC}, \Delta_1 = 1$

Single loop.  $P_{11} = \frac{1}{sL}, P_{21} = -\frac{1}{sR_2C}, P_{31} = -\frac{1}{s^2LC}$

$$\Delta = 1 + \frac{R_1}{sL} + \frac{1}{sR_2C} + \frac{1}{s^2LC}$$

Hence  $\frac{E_c(s)}{E(s)} = \frac{P_1}{\Delta} = \frac{\frac{1}{sR_2C}}{1 + \frac{1}{sR_2C} + \frac{1}{s^2LC}}$

$$= \frac{1}{1 + s\left(R_1C + \frac{L}{R_2}\right) + s^2LC}$$

Q3 (b) Find the overall transfer function of the system in Fig.5.

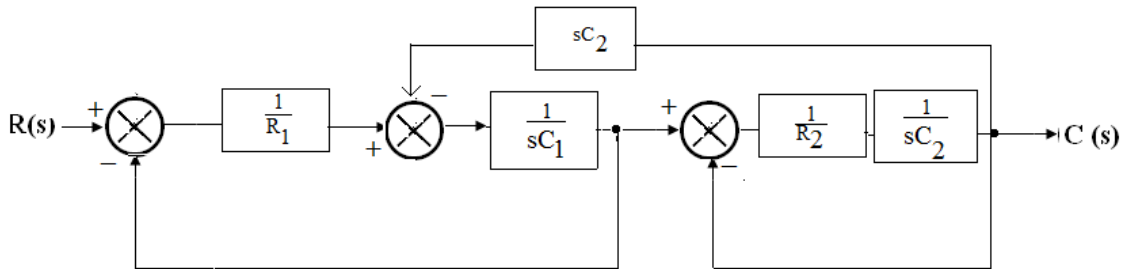
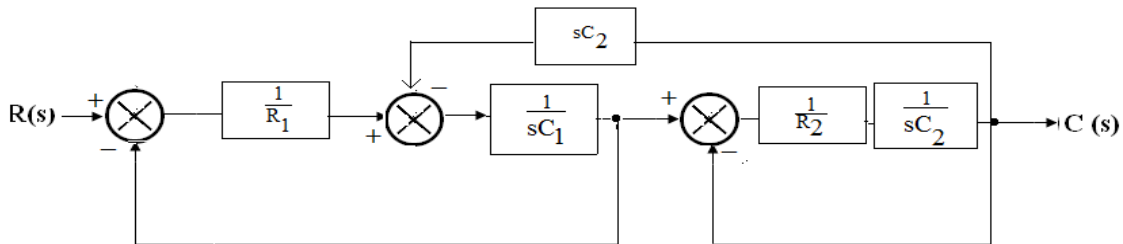


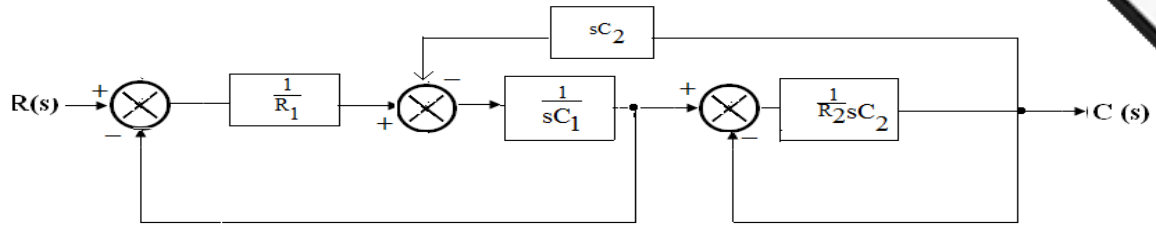
Fig.5

Answer

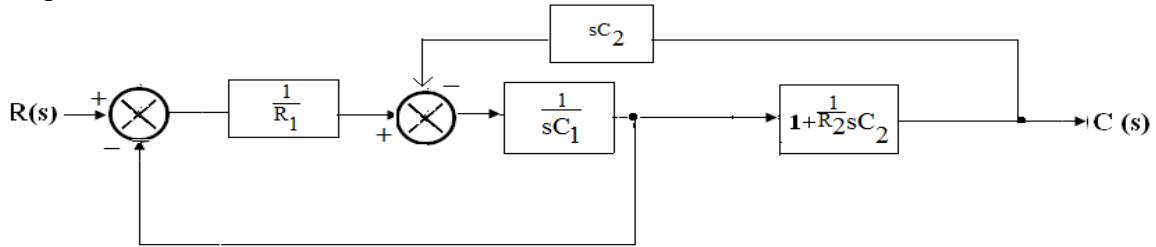
Step1: Shift the pick off point beyond the block  $\frac{1}{sC_2}$



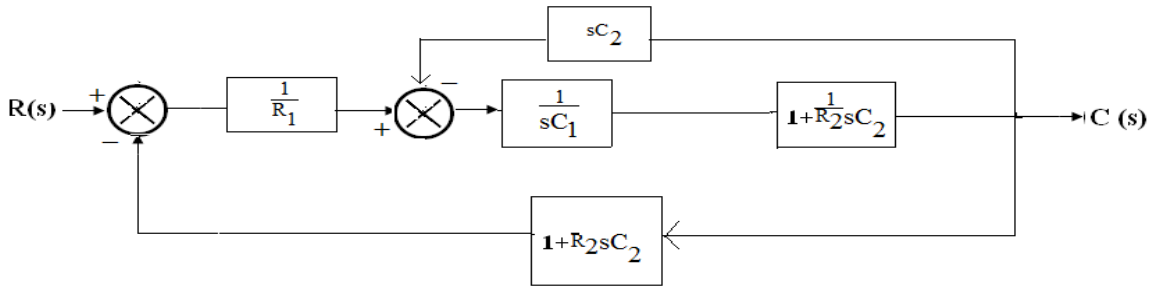
Step2: Two blocks are in cascade



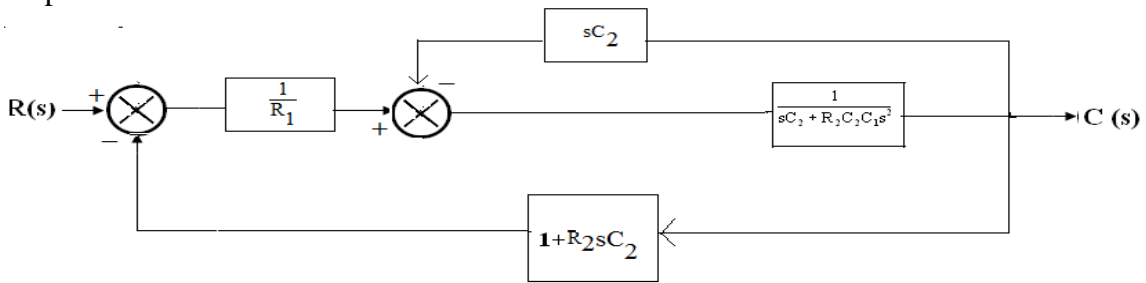
Step3:



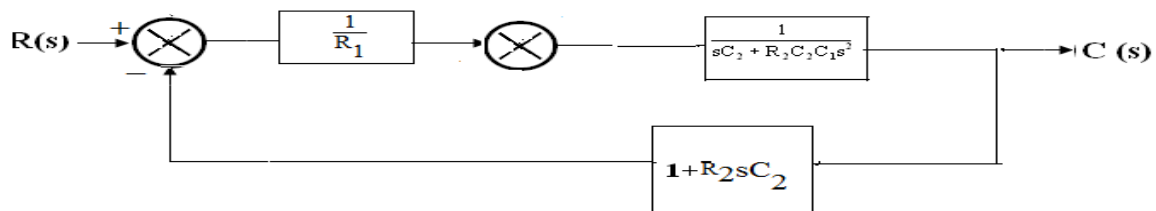
Step4:



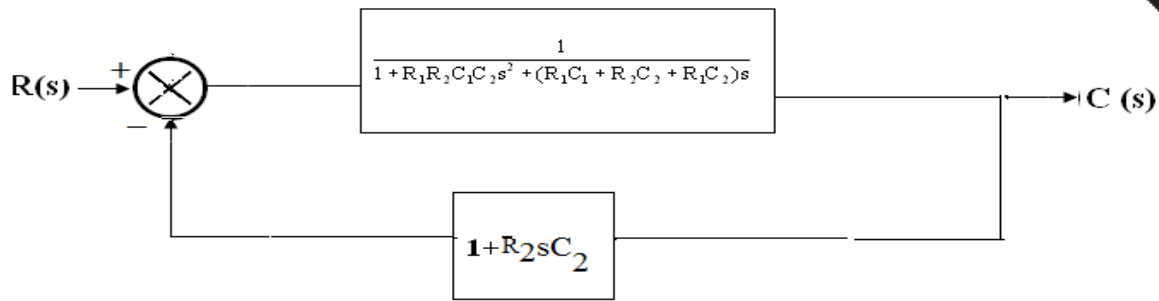
Step5:



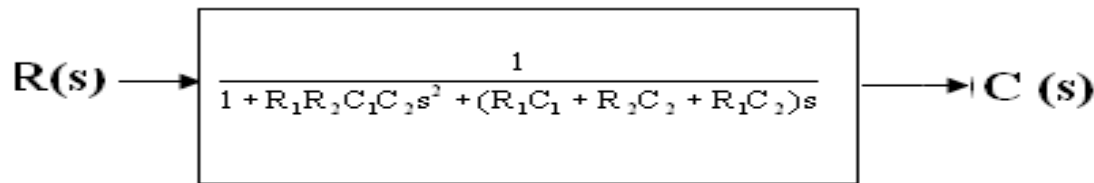
Step6:



Step7:



Step8:



$$\frac{C(s)}{R(s)} = \frac{1}{1 + R_1R_2C_1C_2s^2 + (R_1C_1 + R_2C_2 + R_1C_2)s}$$

**Q4 (a) Explain how the parameter variation is reduced by the use of feedback.**

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**Q4 (b) What are different controller components? Explain in brief.**

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**Q5 (a) A second order system with  $\xi = 0.5$  and  $\omega_n = 6$  rad/sec is subjected to a unit step input. Determine the rise time, peak time, settling time and peak overshoot.**

**Answer**

Given that  $\xi = 0.5$  and  $\omega_n = 6$  rad/sec

$$\text{Rise time } t_r = \frac{\pi - \tan^{-1} \sqrt{1 - \xi^2}}{\omega_n \sqrt{1 - \xi^2}} = 0.403 \text{ sec}$$

$$\text{Peak time } t_p = \frac{\pi}{\omega_n \sqrt{1 - \xi^2}} = 0.605 \text{ sec}$$

$$\text{Settling time } t_s = \frac{4}{\xi \omega_n} = 1.00 \text{ sec}$$

$$\text{Maximum/Peak overshoot} = M_p = e^{-\frac{\pi \xi}{\sqrt{1 - \xi^2}}} \times 100 = 1.63\%$$

**Q5 (b)** The transfer function of a unity feedback system is  $G(s) = \frac{10}{s(s+1)}$ .

Find the dynamic error coefficient and steady state error to the input  $r(t) = P_0 + P_1 t + P_2 t^2$

**Answer**

$$G(s) = \frac{10}{s(s+1)}, H(s) = 1$$

$$\frac{E(s)}{R(s)} = \frac{1}{1+G(s)H(s)} = \frac{s+s^2}{10+s+s^2} \quad (1)$$

$$= 0.1s + 0.09s^2 - 0.019s^3 \dots$$

$$\therefore E(s) = 0.1s R(s) + 0.09s^2 R(s) - 0.019s^3 R(s) \dots$$

Take inverse Laplace

$$e(t) = 0.1 r(t) + 0.09 r(t) - 0.019 r(t) \quad (2)$$

Now

$$r(t) = P_0 + P_1 t + P_2 t^2$$

$$r(t) = P_1 + 2 P_2 t$$

$$r(t) = 2P_2$$

$$r(t) = 0$$

eq. (2) becomes

$$e(t) = 0.1(P_1 + 2P_2 t) + 0.18 P_2$$

The steady state error is

$$\lim_{t \rightarrow \infty} e(t) = \lim_{t \rightarrow \infty} 0.1(P_1 + 2P_2 t) + 0.18 P_2$$

The dynamic error coefficients from eq. (2)

$$K_1 = \frac{1}{0.1} = 10, K_2 = \frac{1}{0.09} = 11.1, K_3 = \frac{1}{-0.019} = -52.63$$

**Q5 (c)** A unity negative feedback control system has open loop transfer function is

$$G(s) = \frac{K(s+1)(s+2)}{(s+0.1)(s-1)}$$

using Routh stability criterion, determine the range

of values of K for which the closed loop system has 0,1 or 2 poles in the right – half of S plane.

**Answer**

The characteristics equation is  $1 + G(s) = 0$

$$(s+0.1)(s-1) + K(s+1)(s+2) = 0$$

$$\text{or } (1+K)s^2 + (3K-0.9)s + (2K-0.1) = 0$$

Apply Routh criterion

$s^2$	1+K	2K-0.1
$s^1$	3K-0.9	
$s^0$	2K-0.1	

(i) No Pole in right half S plane

$$\begin{array}{ll} K + 1 > 0 & \text{or } K > -1 \\ 3K - 0.9 > 0 & K > 0.3 \\ 2K - 0.1 > 0 & K > 0.05 \end{array}$$

(ii) 1 Pole in right half s Plane (= No sign change in first column terms)  
 $-1 < K < 0.05$

(iii) 2 Poles in right half s plane = (two change in sign in first column terms)  
 $0.05 < K < 0.3$

**Q6 (a) The open loop transfer function of feedback system is**

$$\frac{K}{s(s+4)(s^2+4s+20)}. \text{ Draw root locus for this system.}$$

**Answer**

Step1: plot poles & zeros

Poles are at  $s=0, s=-4, s^2+4s+20=0$

$$S = -2 \pm y4$$

Step2: Segment between  $s=0$  and  $s=-4$  is the part of roots focus.

Step3: No of root loci  $N=p=4$

Step4: Centroid of asymptote

Step5: Angle of asymptote

$K=0$	$\varphi_1 = 45^\circ$
$K=1$	$\varphi_2 = 135^\circ$
$K=2$	$\varphi_2 = 225^\circ$
$K=3$	$\varphi_4 = 315^\circ$

Step6: Break point characteristic is  $1 + G(s)H(s) = 0$

$$s^4 + 8s^3 + 36s^2 + 80s + k = 0$$

or

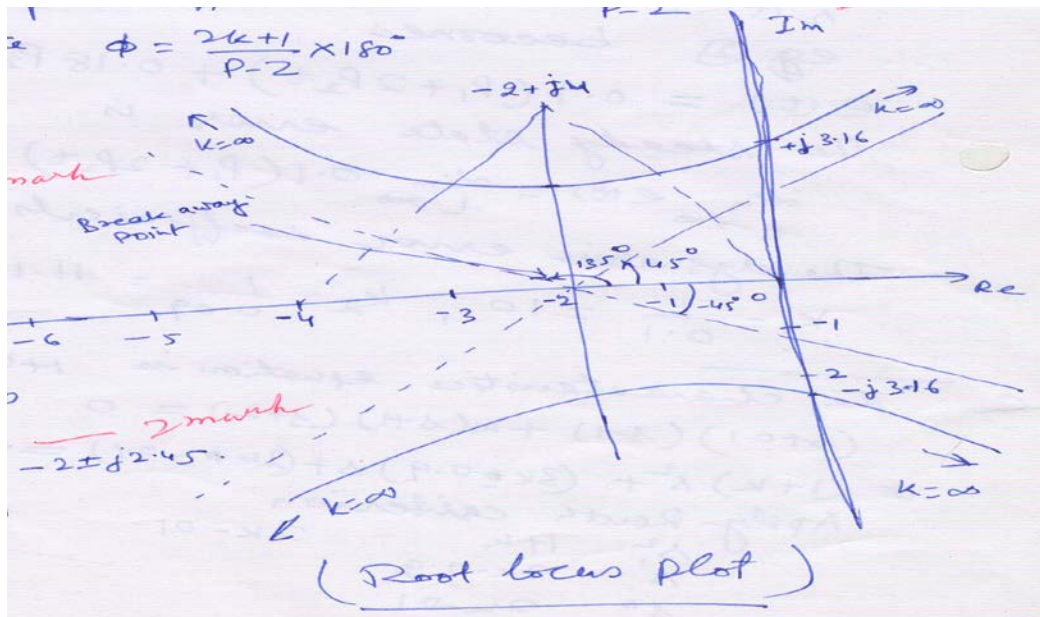
$$k = -(s^4 + 8s^3 + 36s^2 + 80s)$$

$$\frac{dk}{ds} = -(4s^3 + 24s^2 + 72s + 80) = 0$$

∴ Break even point  $s = -2s$

two complex break even points are  $-2 \pm j2.45$

step7 : point of intersection



$s^4$	1	36	K
$s^3$	8	80	
$s^2$	26	K	
$s^1$	$80 - 0.307k$		
$s^0$	k		

$$\text{Maximum/Peak overshoot} = M_p = e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}} \times 100 = 16.3\%$$

Q6 (b) Explain the sensitivity of the roots of the characteristics equation.

Answer





$$a(s) = \frac{10}{s(s+1)}, H(s) = 1$$

$$\frac{E(s)}{R(s)} = \frac{1}{1 + a(s)H(s)} = \frac{s + s^2}{10 + s + s^2} \dots\dots\dots(1)$$

$$= 0.1s + 0.09s^2 \cdot 0.019s^3 \dots\dots\dots$$

$$\therefore E(s) = 0.1sR(s) + 0.09s^2 R(s) - 0.019s^3 R(s) \dots\dots$$

Take inverse laplace

$$e(t) = 0.1r(t) + 0.09r(t) - 0.019r(t) \dots\dots\dots(2)$$

Now

$$r(t) = P_0 + P_1t + P_2t^2$$

$$r(t) = P_1 + 2P_2t$$

$$r(t) = 2P_2$$

$$r(t) = 0$$

$\therefore$  eg...(2) becomes

$$e(t) = 0.1(P_1 + 2P_2t) + 0.18P_2$$

The steady state error is

$$\lim_{t \rightarrow \infty} e(t) = \lim_{t \rightarrow \infty} 0.1(P_1 + 2P_2t) + 0.18P_2$$

The dynamic error coefficients  $e_p(2)$

$$k_1 = \frac{1}{0.1} = 10, k_2 = \frac{1}{0.09} = 11.1, k_3 = \frac{1}{-0.019} = -52.63$$

The characteristics equation is  $1+G(s) = 0$

$$(s+0.1)(s-1)+k(s+1)(s+2) = 0$$

or

$$(1+k) s^2 + (3k-0.9) s + (2k-0.1) = 0$$

Apply Routh criterion

$s^2$	$1+k$	$2k-0.1$
$s^1$	$3k-0.9$	
$s^0$	$2k-0.1$	

For stability  $k > 0$

$$80 - 0.307k > 0 \text{ or } k < 260$$

at  $k=260$ , the auxiliary efn  $A(s) = 26s^2 + k$

$$26s^2 + 260 = 0 \rightarrow s = \pm 3.16j$$

Step8: Angle of departure

$$\phi_d = 180^\circ - (117^\circ + 90^\circ + 63^\circ) = -90^\circ$$

Q7 (a) Why logarithmic scale is used for Bode plot ? Sketch the Bode plot for the transfer function  $H(s) = \frac{1000}{(1+0.1s)(1+0.001s)}$  determine (i) Phase margin (ii) Gain margin.

Answer

put  $s=j\omega$

$$H(j\omega) = \frac{1000}{(1+j\omega \cdot 0.1)(1+j\omega \cdot 0.001)}$$

Starting point is

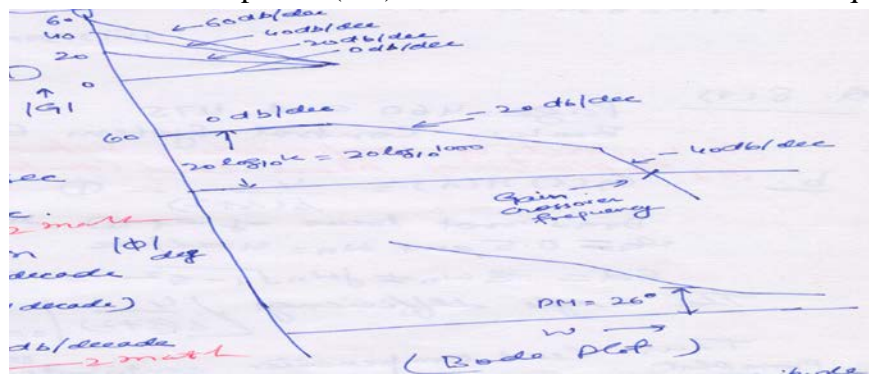
$$20 \log_{10} k = 20 \log_{10} 1000 = 60 \text{db}$$

$$\text{Corner frequency } \omega_1 = \frac{1}{0.1} = 10 \text{ rad/sec}$$

$$\omega_2 = \frac{1}{0.001} = 1000 \text{ rad/sec}$$

Magnitude plot

- (i) Make starting point 60db on y axis & draw a line with slope of 0db/decade
- (ii) Draw a line with slope (0-20=-20 db/decade) from 1<sup>st</sup> corner frequency  $\omega_1$
- (iii) Draw a line of slope  $-20+(-20)=-40$  db/decade from 2<sup>nd</sup> corner frequency  $\omega_2$



Phase plot

$\omega$	$-\text{Arg}(1+j0.1\omega)$	$-\text{arg}(1+j0.001\omega)$	Resultant
50	-76.6	-2.86	-81.46
100	-84.2	-5.7	-90
150	-86.2	-8.5	-94
200	-87.13	-11.3	-98
500	-88.85	-26.56	-115.4
800	-88.85	-38.65	-127.93
1000	-89.28	-45	-134.42
2000	-89.72	-63.43	-153.15
5000	-89.88	-71.56	-161.36
8000	-89.92	-78.69	-168.57
		-82.87	-172.79

Phase Margin:-

→ Throw point of integration of magnitude curve with 0 db draw a line on phase curve. This line into phase curve at  $-154^\circ$

$$\therefore \text{Phase margin } 154^\circ - (-180^\circ) = +26^\circ$$

→ Gain margin =  $\infty$

Since phase margin is  $+26^\circ$  and gain margin is  $\infty$ , the system is inherently stable.

**Q7 (b) The forward path transfer function of a unity feedback control system is**

$G(s) = \frac{100}{(s+6.54)}$  **find the (i) resonance peak (ii) resonance frequency and (iii) bandwidth.**

**Answer**

$$G(s) = \frac{100}{s(s+6.54)}, H(s) = 1$$

$$\frac{c(s)}{R(s)} = \frac{G(s)}{1+G(s)H(s)} = \frac{\frac{100}{s(s+6.54)}}{1 + \frac{100}{s(s+6.54)}} = \frac{100}{s^2 + 6.54s + 100}$$

$$\text{Compare with } \frac{\omega_n^2}{s^2 + 2E\omega_n s + \omega_n^2}$$

$$\omega_n^2 = 100 \Rightarrow \omega_n = 10 \text{ rad/sec}$$

(i) Resonant frequency

$$\omega_r = \omega_n \sqrt{1-2E^2} = 8.86 \text{ rad/sec}$$

$$(ii) \text{ Resonant peak} = \frac{1}{2E\sqrt{1-E^2}} = 1.618$$

$$(iii) \text{ Bandwidth} = \omega_n \sqrt{1-2E^2 + (2-4E^2 + 4E^4)^{1/2}} \\ = 14.34 \text{ rad/sec}$$

**Q8 (a) What is the necessity of compensating network? Explain phase lead compensator and give its comparison with phase lag compensator.**

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**Q8 (b) Design a lead compensator for the system shown in Fig. 6. Given that  $\omega_n = 4 \text{ rad/sec}$  and  $\xi = 0.5$  for compensated system.**

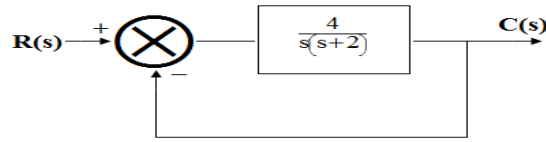


Fig.6

Answer

$$G(s)H(s) = \frac{4}{s(s+2)} \dots\dots\dots(1)$$

Draw root locus of equation (1) it is shown in fig x.

$\zeta = 0.5$ , and  $\omega_n = 4 \text{ rad/sec}$

$$s_d = \zeta \omega_n \pm j\omega_n \sqrt{1 - \zeta^2} = -2 \pm j3.46$$

$$\text{The angle deficiency } \angle \frac{4}{s(s+2)} \Big|_{s=-2 \pm j3.46} = -210^\circ$$

Or

$$180^\circ - (90 + 120) = 30^\circ$$

Thus lead compensator contribute  $\phi = 30^\circ$  at this point

$$\text{From plot Zero at } s = -2.96 \therefore = 2.96 \quad \frac{1}{LT} = 5.5$$

$$\alpha = 0.538$$

Pole at  $s = -5.5 \quad T = 0.337$

The open loop COMPENSATED transfer function of compensated system is

$$G_c(s)G(s) = k_c \frac{s + 2.96}{s + 5.5} \cdot \frac{4}{s(s+2)} = \frac{k^1 (s + 2.96)}{s(s+2)(s+5.5)} \dots\dots\dots(2)$$

$$k^1 = \frac{k^1 (s + 2.96)}{s(s+2)(s+5.5)} \Big|_{s_d = -2 \pm j3.46} = 1 = k^1 = 18.7 k_c = \frac{18.7}{4} = 4.675$$

$$K_{ed} = 4.675 \times 0.538 = 2.52.$$

$$\text{transfer function of lead compensation} = 2.52 \cdot \frac{1 + 0.337s}{1 + 0.182s}$$

or

$$G_c(s) = 4.675 \frac{s + 2.96}{s + 5.5}$$

open loop compensated transfer function of compensated system

$$G_c(s)G(s) = \frac{18.7(s + 2.96)}{s(s+2)(s+5.5)}$$

$$\text{the velocity error constant } k_v = \lim_{s \rightarrow 0} s G_c(s)G(s) = \lim_{s \rightarrow 0} \frac{s \cdot 18.7(s + 2.96)}{s(s+2)(s+5.5)}$$

$$= k_v = 5.02 \text{ sec}^{-1}$$

**Q9 (a)** A system with state model is 
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} \mathbf{u}$$

Where  $\mathbf{u}(t)$  is unit step occurring at  $t = 0$  and  $\mathbf{x}^T(0) = [1 \ 0]$ . Obtain the time response of the system and compute state transition matrix.

**Answer**

$$\mathbf{A} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix}; \mathbf{B} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$

State transitions matrix  $\phi(t) = 1 + \mathbf{A}t + \frac{1}{2!} \mathbf{A}^2 t^2 + \frac{1}{3!} \mathbf{A}^3 t^3$

Substituting values of a, we get

$$e^{\mathbf{A}t} = \begin{bmatrix} 1+t+0.5t^2+\dots & 0 \\ t+t^2+\dots & 1+t+0.5t^2+\dots \end{bmatrix} = \begin{bmatrix} \phi_{11} & \phi_{12} \\ \phi_{21} & \phi_{22} \end{bmatrix}$$

$$\phi(t) = \begin{bmatrix} e^t & 0 \\ te^t & e^t \end{bmatrix}$$

Time response of the system is

$$\mathbf{x}(t) = \begin{bmatrix} \mathbf{x}_0 + \int_0^t \phi(-t)\mathbf{B}u dt \end{bmatrix}$$

$$\phi(-t)\mathbf{B}u = \begin{bmatrix} e^{-t} & 0 \\ te^{-t} & e^{-t} \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} e^{-t} \\ e^{-t}(1-t) \end{bmatrix}$$

$$\mathbf{x}(t) = \begin{bmatrix} e^t & 0 \\ te^t & e^t \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} + \begin{bmatrix} 1 & -e^{-t} \\ t & e^{-t} \end{bmatrix} = \begin{bmatrix} 2e^t - 1 \\ 2e^t \end{bmatrix}$$

**Q9 (b)** Test the following system for controllability and observability.

$$\dot{\mathbf{x}} = \begin{bmatrix} -3 & 1 & 1 \\ -1 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 & 1 \\ 0 & 0 \\ 2 & 1 \end{bmatrix} \mathbf{u} \quad \text{and} \quad \mathbf{y} = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 1 & 0 \end{bmatrix} \mathbf{x}.$$

**Answer**

$$\mathbf{A} = \begin{bmatrix} -3 & 1 & 1 \\ -1 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}, \mathbf{B} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \\ 2 & 1 \end{bmatrix}, \mathbf{C} = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 1 & 0 \end{bmatrix}$$

$$[A \ B] = \begin{bmatrix} 2 & -3+1 \\ 2 & -1+1 \\ 2 & 1 \end{bmatrix} = \begin{bmatrix} 2 & -2 \\ 2 & 0 \\ 2 & 1 \end{bmatrix}$$

$$[A^2B] = \begin{bmatrix} -3 & 1 & 1 \\ -1 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 2 & -2 \\ 2 & 0 \\ 2 & 1 \end{bmatrix} = \begin{bmatrix} -2 & 7 \\ 0 & 3 \\ 2 & 1 \end{bmatrix}$$

$$Q_c = [B \ AB \ A^2B]$$

$$= \begin{bmatrix} 012 & -2 & -27 \\ 002 & 003 \\ 212 & 121 \end{bmatrix} \quad Q_c \text{ has Rank}=3, \text{ thus system is controllable}$$

Test for Observability:-

$$A = \begin{bmatrix} -3 & 1 & 1 \\ -1 & 0 & 1 \\ 0 & 0 & 1 \end{bmatrix}, C = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 1 & 0 \end{bmatrix}$$

$$C^T = \begin{bmatrix} 0 & -4 \\ 0 & 1 \\ 1 & 2 \end{bmatrix}, A^T = \begin{bmatrix} -3 & -1 & 0 \\ 1 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

$$A^T C^T = \begin{bmatrix} 0 & -4 \\ 0 & 1 \\ 1 & 2 \end{bmatrix}, (A^T)^2 C^T = \begin{bmatrix} 0 & 11 \\ 0 & -4 \\ 1 & 1 \end{bmatrix}$$

$$Q_o = [C^T : A^T C^T : (A^T)^2 C^T] = \begin{bmatrix} 010 & -40 & 11 \\ 010 & 10 & -4 \\ 101 & 21 & -1 \end{bmatrix}$$

$$\text{Check for Rank} = \begin{bmatrix} -4 & 0 & 11 \\ 1 & 0 & -4 \\ 2 & 1 & -1 \end{bmatrix} = -5 \text{ is not equal to } 0$$

Rank of  $Q_o = 3$ , Thus System is completely Observable

### Text Book

**Control Systems Engineering, I.J. Nagrath and M. Gopal, Fifth Edition (2007 New Age International Pvt. Ltd.**